MEMORANDUM



Missouri Department of Transportation Construction - Materials Central Laboratory

TO: Allen Lane-sl/gs

CC/ATT: Mark Croarkin-sl/mt

Larry Carver-co/gs Mark Simon-sl/cm

FROM: Thomas W. Fennessey

Geotechnical Engineer

DATE: August 5, 2015

SUBJECT: Materials

Geotechnical Section

Foundation Investigation for Beaufort Maintenance Building

Job No. R35G-FI2315 Franklin County

General – It is understood that a single-story maintenance building is proposed to be constructed on the MoDOT maintenance lot in Beaufort, Missouri to the south of the existing maintenance building along MO185. No grading plan has been provided although it is anticipated that the finished grade will be near the existing ground surface elevation at the western side of the proposed building (about Elev. 762.5 ft.), which is higher than the existing ground elevation at the eastern side of the proposed building. Thus, it is anticipated that across most of this site, the grade will be raised about 0.0 to 2.0 feet.

A site plan for this proposed building is provided as Figure 1. In addition to the utilities shown on Figure 1, it is also understood that there is an existing waterline whose location is not exactly known but reported to run somewhere under the eastern half of the proposed building. It is also understood from preliminary plans that foundation design is based upon an assumed soil bearing pressure of 2000 psf. The preliminary plans also indicate the building is to be supported on strip footings under the perimeter stem walls. The preliminary plans show these proposed strip footings to be 2.0 feet wide and bear at 2.5 feet below finished grade. No additional information regarding foundation loads or settlement criteria for this proposed building has been provided.

Four borings were drilled for this proposed building with one boring being drilled near each corner as indicated on Figure 2 - Boring Location Aerial. A subsurface profile of these borings is included as Figure 3. Also attached are individual boring logs for each of the locations drilled.

<u>Subsurface Conditions</u> – Across the site, the subsurface conditions encountered varied somewhat from boring location to boring location. In general though, fill and possible fill of varying description, strength, and thickness were found to overlie relatively shallow stiff to dense natural soils and highly weathered rock materials across the site.

At Boring T-15-50 (Elev. 762.3 feet), near the northwest corner of the proposed building, about 1.0 feet of asphalt and crushed aggregate base fill was found to overlie very stiff (Pocket Penetrometer = 3.50 tsf)

fat clay to lean clay possible fill to about 3.0 feet. This was underlain by very stiff native soils and then highly weathered rock materials below about 5.1 feet.

At Boring T-15-51 (Elev. 762.4 feet), near the southwest corner of the proposed building, about 1.5 feet of crushed aggregate base fill was found to overlie medium stiff to stiff (Pocket Penetrometer = 0.75-1.50 tsf) lean clay possible fill to about 4.5 feet. This was underlain by medium stiff to stiff native soils and then highly weathered rock materials below 6.0 feet.

At Boring T-15-52 (Elev. 760.8 feet), near the southeast corner of the proposed building, about 4.5 feet of stiff to very stiff (Pocket Penetrometer = 1.75-2.25 tsf) lean clay possible fill was found to overlie very stiff native soils and then highly weathered rock below 7.9 feet.

At Boring T-15-53, near the northeast corner of the proposed building, about 1.2 feet of asphalt and crushed aggregate base fill was found to overlie medium stiff (Pocket Penetrometer = 0.50-0.75 tsf) lean clay possible fill to about 4.5 feet. This was underlain by dense and very stiff native soils and then highly weathered rock materials below about 10.5 feet. Additionally at this location, it was noted that the moisture content is 27% and the plastic limit is 17% in this possible fill. This would suggest that the existing moisture content is significantly above the optimum moisture content for compaction for this possible fill since optimum moisture content is typically slightly less than the plastic limit.

Recommendations – As indicated above, it is understood from preliminary plans that foundation design is based upon an assumed soil bearing pressure of 2000 psf. However, not all of the existing soils encountered across the proposed building site are capable of providing this assumed bearing pressure. Due to the presence of the medium stiff (Pocket Penetrometer = 0.50-0.75 tsf) possible fill encountered at Boring T-15-53, near the northeast corner of the proposed building, the actual allowable bearing pressure would be limited to 1000 psf without some improvement to the existing fill soils in this vicinity.

In this vicinity, along the eastern edge of the paved maintenance lot, it is suspected that older fill was potentially placed without proper compaction resulting in softer soils along the edge of the lot. Alternately, this area of softer and wetter soils could also be due to a leaking water line that is reported to run somewhere in the vicinity of the boring location. No similarly soft or overly wet conditions were noted at the other boring locations across the site and apparent recent fill material at the boring location near the proposed southeast building corner and apparent older fill material at the boring locations near the proposed northwest and southwest building corners have adequate density and strength to provide the assumed bearing capacity.

Therefore, it is recommended to improve the existing fill materials that fall under that portion of the eastern wall and that portion of the northern wall along the eastern edge of the existing paved portion of the maintenance lot where existing fill materials have an undrained shear strength of less than 1250 psf. This would require that unimproved existing fill soils have a pocket penetrometer reading of at least 1.25 tsf or can only be indented slightly by thumb with moderate effort. Any existing soils not meeting these criteria should be improved by excavating, adjusting moisture content as appropriate, and recompacting to a depth of at least one footing width below and at least one-half footing width either side of the proposed strip footing. For the proposed 2-foot wide footing bearing 2.5 feet below finished grade, this would require improvement of existing soft fill to a depth of 4.5 feet below finished grade and 3.0 feet either side of centerline of the strip footing.

Allen Lane Page 3 August 5, 2015

In addition to the ground improvement recommendation above, the following additional recommendations are also provided.

- Proof roll any building areas to receive fill with a fully loaded tandem axle dump truck prior to fill placement. Any areas exhibiting pumping or rutting should be undercut and backfilled with properly compacted fill.
- Prior to placement of any new fill, scarify the surface of any area to be filled. Any areas to be filled with an existing slope of 6H:1V or steeper should be benched prior to placement of new fill.
- It is recommended that fill material be lean clay or better. Fill should be compacted to 95% of standard Proctor maximum dry density. Non-granular fill material should be compacted at or within 3% of optimum moisture content. All fill and cut slopes should be constructed to slope and drain away from the proposed building.
- If non-granular fill material is used, at least 10 inches of crushed aggregate base should be placed above the non-granular fill in non-paved traffic areas outside the proposed building to bring the surface to final grade.
- An allowable bearing pressure of 2000 psf or less may be used for the design of strip footings constructed on or in properly compacted fill including existing and improved fill soils at this site. Shallow foundations shall be embedded at least 24 inches below finished grade for frost protection. Strip footings shall have a minimum width of 1.5 feet.

cs j:\sublec\tom\beaufort maintenance building ltr.doc Attachments

Missouri Department of Transportation Construction and Materials

Design: Skew: Location: 6697 Highway 185 South, Ended Donahoe Bent: Logged By: Thomas Fennessey Operator: Michael Donahoe Station: Northing: 939465.0 Date of Work: 07/23/15-07/23/15 Offset: Easting: 622952.9 Depth to Water: Elevation: 762.3 Requested Northing: 939465.0 Depth Hole Open: Requested Station: Requested Easting: 622955.9 Time Change: Requested Offset: Equipment: CME 45 ,Split-Spoon Sampler Requested Elevation: 762.3 Location Note: Offset 3.0 ft. W, 0.0 ft. N, and 0.0 ft. El. from staked NW Building Corn Drill No.: G-9577 Hammer Efficiency: 84% Drilling Method: Hollow Stem Auger	ner
Station: Northing: 939465.0 Date of Work: 07/23/15-07/23/15 Offset: Easting: 622952.9 Depth to Water: Elevation: 762.3 Requested Northing: 939465.0 Depth Hole Open: Requested Station: Requested Easting: 622955.9 Time Change: Requested Offset: Equipment: CME 45 , Split-Spoon Sampler Requested Elevation: 762.3 Location Note: Offset 3.0 ft. W, 0.0 ft. N, and 0.0 ft. El. from staked NW Building Corn Drill No.: G-9577 Hammer Efficiency: 84% Drilling Method: Hollow Stem Auger	ner
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Requested Station: Requested Easting: 622955.9 Time Change: Full Properties of the Change: Fu	ner
Requested Offset: Equipment: _CME 45 ,Split-Spoon Sampler Requested Elevation: _762.3 Location Note: _Offset 3.0 ft. W, 0.0 ft. N, and 0.0 ft. El. from staked NW Building Corn Drill No.: _G-9577 Hammer Efficiency: _84% Drilling Method: _Hollow Stem Auger	ner
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Drill No.: G-9577 Hammer Efficiency: 84% Drilling Method: Hollow Stem Auger	
L de la company	Tests
C G Str St	Tests
Graphic (ft) Graphic Graphic Graphic Graphic Graphic Graphic Sample Type REC % (RQD %) Shear Data Shear Data Field Tests	Index Tests
0 0.0-1.0' ASPHALT and CRUSHED AGGREGATE BASE	
1.0-5.1' Reddish brown, FAT CLAY to lean clay, scattered gravel, trace sandstone fragments, very stiff, moist 1.0-3.0' Possible Fill	
67 4-4-9 (18) PP = 3.50 tsf	MC = 18.7% γ _{sat} = 132 pcf ⁽¹⁾ LL = 49 PL = 17
5.1-8.1' Sandstone, light tan to light reddish	
brown, extremely soft, highly weathered, dry 93 11-19-15 (48)	
755	
8.1-9.5' Dolomite, light gray, extremely soft to medium hard, highly weathered, dry 8.5-8.6' Dark Reddish Brown Shale	
9.5-10.4' Sandstone, white to light reddish brown, extremely soft, highly weathered, dry	
Bottom of borehole at 10.4 feet.	

(1) = Assumed, (2) = Actual

LETTER BOREHOLE - R35G-S2109.GPJ - 7/31/15 11:03 - J:\SG\GINT\PROJECT FILES\R35G-FI2315.GPJ

Coordinate System: Modified U.S. State Plane 1983 Coordinate Zone: Missouri East Coordinate Proj. Factor: 1.000064904 Coordinate Datum: NAD 83 (CONUS) Coordinate Units: U.S. Survey Feet

^{*} Persons using this information are cautioned that the materials shown are determined by the equipment noted and accuracy of the "log of materials" is limited thereby and by judgement of the operator. THIS INFORMATION IS FOR DESIGN PURPOSES ONLY.

Missouri Department of Transportation Construction and Materials

Job N	o.: _R	35G-FI2315 C	county: Fra	nklin				Route: _185			
Desig	n:		Skew:					Location: 6697 Highway 185 South, Beaufort, MO			
			.ogged By:	Thoma	as Fe	nnessey	<u>'</u>	Operator: Michae	l Donahoe		
			lorthing: 9	39310.	1			Date of Work: _07/			
			asting: 62					Depth to Water:			
								Depth Hole Open:			
			· Requested E					Time Change:			
			quipment:	_							
								0.0 ft. El. from Stake			
_			lammer Effic					Drilling Method:			
Depth (ft)	Graphic	Description		Elevation (ft)	Sample Type	REC % (RQD %)	Blow Counts (N_{60})	Shear Data	Field Tests	Index Tests	
0	. • •	0.0-1.5' CRUSHED AGGREGATE	RASE								
5		1.5-4.5' Light gray, LEAN CLAY, m to stiff, moist, Possible Fill 4.5-6.0' Brown, SANDY LEAN CLASTIFF to stiff, moist 6.0-10.3' Sandstone, reddish brown tan, extremely soft, highly weathered Bottom of borehole at 10.3	edium stiff Y, medium n to light ed, dry	760		93 67	2-2-2 (6) 2-7-15 (31) 8-15/0.4', 10/0'		PP = 0.75 tsf PP = 1.50 tsf PP = 1.00 tsf PP = 1.50 tsf	MC = 14.6% γ _{sat} = 137 pcf ⁽¹⁾ LL = 29 PL = 15	
N = (F	-m/60\N	Im N _{co} - Corrected N value for standard 60%	SDT officionay	· Em M	logeur	od hamma	or officionav in no	roont: Nm. Observed N	valuo		

(1) = Assumed, (2) = Actual

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Missouri Department of Transportation Construction and Materials

Job N	o .: _R	35G-FI2315	County: Fra	nklin				Route: <u>185</u>				
Design: Skew:								Location: 6697 Highway 185 South, Beaufort, MO				
Bent:			Logged By:	Thoma	as Fe	nnessey	<u>'</u>	Operator: Michael Donahoe				
Statio	n:		Northing: 93	39310.	6			Date of Work: 07/23/15-07/23/15				
Offset	t:		Easting: 62	2996.5				Depth to Water: Depth Hole Open:				
Eleva	tion: _	760.8	Requested N	orthing	j: _93	39310.6						
Requested Station: Re			Requested E	asting:	623	3012.5		Time Change:				
Requ	ested (Offset:	Equipment:	CME 4	45 ,S _l	olit-Spoo	n Sampler					
Requ	ested E	Elevation: 756.8	Location Not	e: Off	set 1	6.0 ft. W	, 0.0 ft. N, and	+4.0 ft. from staked	SE Building Con	ner due to slope		
Drill N	lo.: _C	9-9577	Hammer Effic	ciency:	_84°	%		Drilling Method: _	Hollow Stem Auge	er		
O Depth (ft)	Graphic	Description		Elevation (ft)	Sample Type	REC % (RQD %)	Blow Counts (N ₆₀)	Shear Data	Field Tests	Index Tests		
		0.0-4.5' Brown to grayish brown, I trace gravel, stiff to very stiff, mois Fill	EAN CLAY st, Possible	760								
				 		60	2-3-2 (7)		PP = 2.25 tsf PP = 1.75 tsf	MC = 12.8% γ_{sat} = 140 pcf ⁽¹⁾ LL = 32 PL = 16		
5		4.5-7.9' Brown, SANDY LEAN CL stiff, moist		755			1-3-5 (11)		PP = 2.50 tsf			
10		7.9-10.3' Sandstone, reddish brov tan, extremely soft to very soft, his weathered, moist to dry Bottom of borehole at 10.3	ghly			93	11-25-30 (77)					
$N_{60} = (1)$	Em/60)N	Im N ₆₀ - Corrected N value for standard 609	6 SPT efficiency	; Em - N	1easur	ed hamme	er efficiency in per	rcent; Nm - Observed N	i-value			

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Design: Skew:								Location: 6697 Highway 185 South, Beaufort, MO			
Bent:			Logged By:	Thom	as Fe	nnessey	<u>/</u>	Operator: Michael Donahoe			
Statio	n:		Northing: 9	39473.	9			Date of Work: 07/23/15-07/23/15			
Offset: Easting: _623)			Depth to Water:			
Elevation: 760.8 Requested N					g: _93	39465.6		Depth Hole Open:			
Reque	ested S	Station:	Requested E	asting	: 623	3010.9		Time Change:			
		Offset:	Equipment:								
-		Elevation: 760.4						+0.4 ft El. from sta	ked NE Building Co	orner due to parked v	
		G-9577	Hammer Effic						Hollow Stem Aug		
Depth (ft)	Graphic	Description		Elevation (ft)	Sample Type	REC % (RQD %)	Blow Counts (N ₆₀)	Shear Data	Field Tests	Index Tests	
0		0.0-1.2' ASPHALT and CRUSHE AGGREGATE BASE	ED .	760							
		1.2-4.5' Grayish brown, LEAN Conganics, medium stiff, moist, Po		- -	_						
		4.5-7.0' Reddish brown, CLAYE'		 		73	2-1-1 (3)		PP = 0.50 tsf PP = 0.75 tsf	MC = 27.0% γ_{sat} = 123 pcf ⁽¹⁾ LL = 31 PL = 17	
_ 5		dense, dry	r GRAVEL, .	755		80	10-16-8 (34)				
		7.0-10.5' Reddish brown, SAND' CLAY, very stiff, moist, interlaye SANDSTONE, extremely soft, hi weathered, dry	red white			93	3-6-11 (24)				
10_		10.5-11.0' Shale, white to dark re	eddish brown,	750		87	4-6-36		PP = 5.00 tsf		
		 extremely soft, moist 11.0-12.3' Sandstone, light tan to brown, extremely soft, highly we 	o light reddish athered, dry	- -			(59)		PP = 5.50 tsf		
		12.3-14.0' Shale, dark reddish bi extremely soft, moist	rown,			87	6-18-17 (49)		PP = 7.50 tsf PP = 8.50 tsf		
_		Bottom of borehole at 14	.0 feet.								

 N_{60} = (Em/60)Nm N_{60} - Corrected N value for standard 60% SPT efficiency; Em - Measured hammer efficiency in percent; Nm - Observed N-value (1) = Assumed, (2) = Actual

 Coordinate System:
 Modified U.S. State Plane 1983
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KEY TO SYMBOLS

CLIENT MoDOT Saint Louis District

PROJECT NAME Beaufort Maintenance Building

PROJECT NUMBER R35G-FI2315

PROJECT LOCATION 6697 Highway 185 South, Beaufort, MO

LITHOLOGIC SYMBOLS (Unified Soil Classification System)



ASPHALT: Asphalt



CH: USCS High Plasticity Clay



CL: USCS Low Plasticity Clay



CLS: USCS Low Plasticity Sandy Clay



DOLOMITE: Dolomite



GC: USCS Clayey Gravel



GW: USCS Well-graded Gravel



SANDSTONE: Sandstone



SHALE: Shale

SAMPLER SYMBOLS



Split-Spoon Sampler

WELL CONSTRUCTION SYMBOLS

ABBREVIATIONS

LL - LIQUID LIMIT (%)

PI - PLASTIC INDEX (%)

W - MOISTURE CONTENT (%)

DD - DRY DENSITY (PCF)

NP - NON PLASTIC

-200 - PERCENT PASSING NO. 200 SIEVE

PP - POCKET PENETROMETER (TSF)

TV - TORVANE

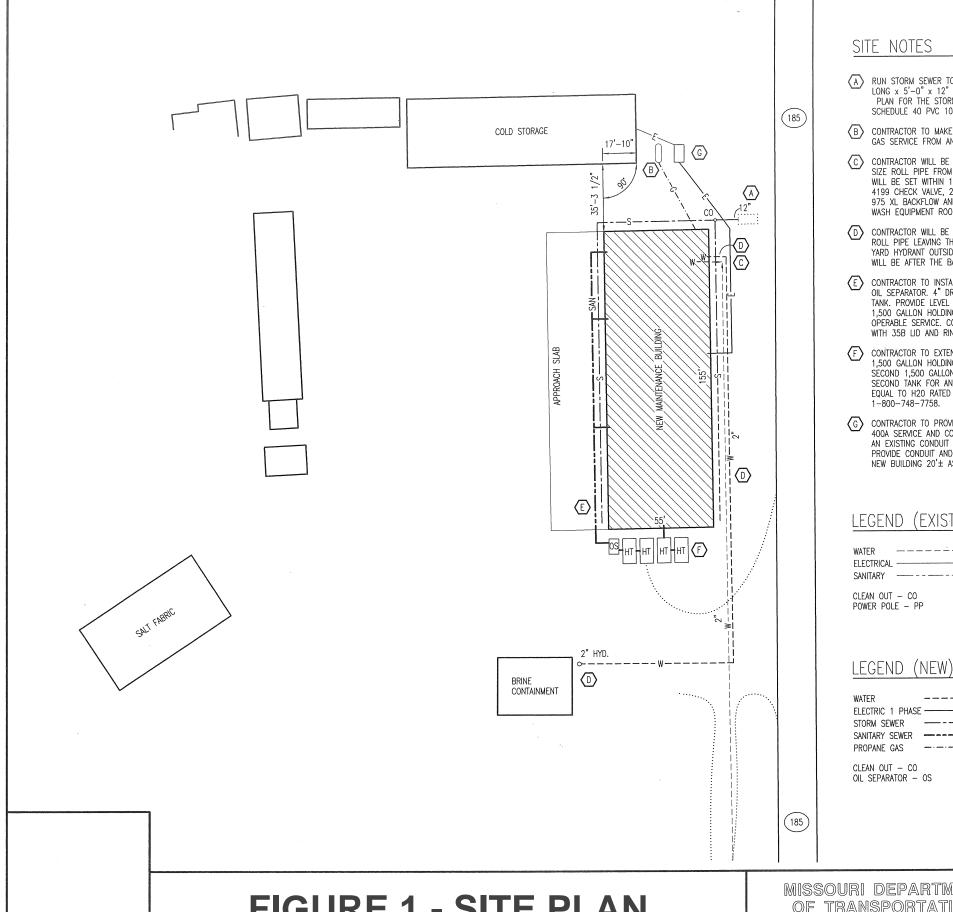
PID - PHOTOIONIZATION DETECTOR

UC - UNCONFINED COMPRESSION

ppm - PARTS PER MILLION

▼ Water Level at End of Drilling

▼ Water Level after Drilling



SITE NOTES

- (A) RUN STORM SEWER TO DAYLIGHT. CONTRACTOR TO PROVIDE 8'-0" LONG x 5'-0" x 12" DEEP (4" DIA. ROCK) RIP-RAP. SEE PLUMBING PLAN FOR THE STORM SCHEDULE 35 PVC SIZE(S). CHANGE TO SCHEDULE 40 PVC 10'-0" BEFORE DAYLIGHTING
- (B) CONTRACTOR TO MAKE CONNECTION AS REQUIRED FOR AN OPERABLE GAS SERVICE FROM AN EXISTING 1,000 GALLON PROPANE TANK.
- C CONTRACTOR WILL BE REQUIRED TO TIE INTO AN EXISTING 2" COPPER SIZE ROLL PIPE FROM WHERE WATER COMPANY'S SERVICE PLACED PIPE WILL BE SET WITHIN 10'± OF THE BUILDING FOOTPRINT. A 2" BADGER 4199 CHECK VALVE, 2"AWWA, CLASS 2 METER AND A 2" WILKENS ZURN, 975 XL BACKFLOW AND 2"PRV VALVE WILL BE REQUIRED INSIDE THE WASH EQUIPMENT ROOM.
- (D) CONTRACTOR WILL BE REQUIRED TO TIE INTO THE 2" COPPER SIZED ROLL PIPE LEAVING THE NEW BUILDING HEADING TO AN EXISTING 2" YARD HYDRANT OUTSIDE THE BRINE CONTAINMENT. THE CONNECTION WILL BE AFTER THE BACKFLOW PREVENTER INSIDE.
- (E) CONTRACTOR TO INSTALL 4" PVC SANITARY SEWER LINE TO AN NEW OIL SEPARATOR. 4" DRAIN LINE TO THE FIRST 1,500 GALLON HOLDING TANK. PROVIDE LEVEL ALARM. THEN PROVIDE 4" DRAIN LINE TO SECOND 1,500 GALLON HOLDING TANK, FLOW LINES AS REQUIRED FOR AN OPERABLE SERVICE, CONCRETE HOLDING TANKS EQUAL TO H20 RATED WITH 35B LID AND RING BY MURDON CORP. 1-800-748-7758.
- F CONTRACTOR TO EXTEND 4" PVC SANITARY SEWER LINE TO A NEW 1,500 GALLON HOLDING TANK. THEN PROVIDE 4" DRAIN LINE TO A SECOND 1,500 GALLON HOLDING TANK. PROVIDE LEVEL ALARM IN THE SECOND TANK FOR AN OPERABLE SERVICE, CONCRETE HOLDING TANKS EQUAL TO H20 RATED WITH 35B LID AND RING BY MURDON CORP. 1-800-748-7758.
- G CONTRACTOR TO PROVIDE NEW ELECTRICAL SERVICE BEGINNING WITH 400A SERVICE AND COOP PROVIDED DISCONNECT AT EXISTING H-FRAME. AN FXISTING CONDUIT SWEEP IS AT THE BASE OF THE H-FRAME. PROVIDE CONDUIT AND CONDUCTORS FROM EXISTING SWEEP INTO THE NEW BUILDING 20'± AS REQUIRED FOR A FUNCTIONAL SERVICE.

LEGEND (EXISTING)

WATER		W
ELECTRICAL		E
SANITARY		SAN
CLEAN OUT	- CO	ELECTRICAL METER - M

POWER POLE - PP

WATER	
ELECTRIC 1 PHASE	E
STORM SEWER	s
	SAN
PROPANE GAS	
CLEAN OUT - CO	HOLDING TANK - HT

SCALE: 1" = 50'-0"

GRADING NOTES:

CONTRACTOR WILL BE RESPONSIBLE FOR:

ALL BACK FILL MATERIAL INSIDE AND OUTSIDE NEW BUILDING.

CRUSHED ROCK BASE UNDER BUILDING & APPROACH SLAB.

BACK FILL ALONG APPROACH SLAB A MINIMUM OF 6" BELOW

PROVIDE TOP SOIL, FERTILIZE, SEED AND STRAW AT ALL THE

MODOT TO HAVE THE FOUR CORNERS STAKED AND BUILDING

EXCAVATED SOIL NOT USED CAN BE PLACED ON SITE. AREA

PROVIDE FINISHED GRADE MATERIAL DISTURBED DURING

FINISHED GRADE TO DRAIN AWAY FROM BUILDING.

LAWN AREAS DISTURBED DURING CONSTRUCTION.

VERIFY UTILITY LOCATIONS BEFORE CONSTRUCTION.

FOOTPRINT & EXTERIOR APPROACH SLAB LEVELED.

EXCAVATION OF THE SUB GRADE.

TOP OF SLAB AND SIDEWALK.

CONSTRUCTION TO MATCH EXISTING.

TO BE DESIGNATED BY OWNER.

EXCAVATING OF FOOTINGS.



FIGURE 1 - SITE PLAN

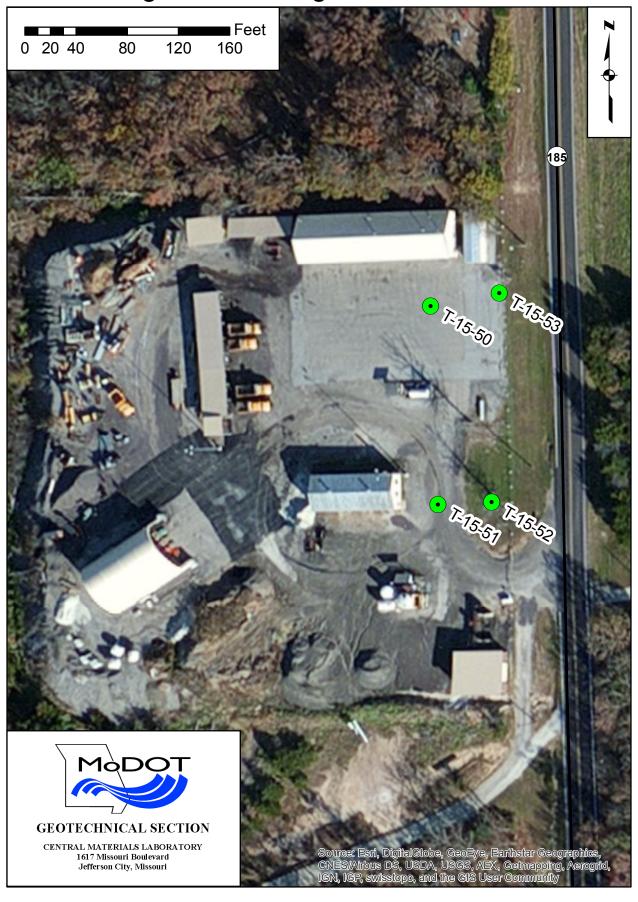
MISSOURI DEPARTMENT OF TRANSPORTATION

> DIVISION OF GENERAL SERVICES FACILITIES MANAGEMENT

Beaufort Maintenance Building St. Louis District - Franklin County 6697 Highway 185 South, Beaufort, MO DATE: 7-17-15

DESIGN BY: LARRY CARVER

Figure 2 - Boring Location Aerial



	Saint Louis Dist			PF PF	USCS Well-graded Gravel	Shale				
			T-15-51 (SW)	N60 (bpf)	pp (tsf)	N60 (bpf)	PP (tsf)	T-15-50 (NW)		
Γ-15-52 (SE)	N60 (bpf)	PP (tsf)							N60 (bpf)	pp (tsf)
				6	0.75-1.50	18	3.50			
	7	1.75-2.25		31	1.00-1.50	48			3	0.50-0.75
	11	2.50		100+		43			34	·········· <u></u> ·······
	11			100+		100+			24	
	100+								59	5.0-5.5
									49	7.5-8.5