

October 29, 2021

ADDENDUM # 3 Little Hills Expressway and Mel Wetter Parkway Intersection Improvements PROJECT NUMBER CMAQ #4917(602) BID # 4527

ATTENTION ALL PLAN HOLDERS:

The City of St. Charles is issuing this Addendum to the Little Hills Expressway and Mel Wetter Parkway Intersection Improvement Plan Sheets and Bid Documents. The purpose of the addendum is to make modifications to the stamped brick median, traffic control plans, sign posts, and the MSE wall. The revised bid information is as follows:

- 1. On the plan sheet #3, the typical section for the median has changed to clarify that Type 5 Aggregate is incidental to the median. The call out for "Stamped Brick Median" has changed to "Pigmented and Textured Median" to match the bid item.
- 2. On plan sheets #12-16, the traffic control plan for phase 1 & 2 changed. Phase 1 added a quality for temporary asphalt on the east and west ends of the roundabout in order to shift westbound traffic into the roundabout for phase 2. Phase 2 plan sheets shows the necessary traffic control to navigate westbound drivers to utilize the northern portion of the roundabout.
 - a. JSP B Work Zone Traffic Management Plan section 4.2-4.2.2 have been revised to reflect these modifications.
 - b. Plan Sheets 2A, 2B and #11 have been updated.
 - c. A temporary asphalt pavement detail has been added to plan sheet #3.
- 3. On plan sheet #20, general note #2 removed ornamental with square tube posts. Also, an extra note #4 was added, stating, "Wayfinding signs shall be mounted on two sign post each".
 - a. JSP Q Roadway Signs/Sign Posts, section 1.3 removed u-channel post and replaced with black square tube post



- 4. On plan sheet #24, the mechanically stabilized earth (MSE) wall height was shortened which reduced the MSE quantity from 8,802 to 5,894 SQFT. Soil reinforcement length changed from .7H to 1.0H which is shown on plan sheet #25.
 - a. Plan Sheets #2A, #2B, #4, #5, Cross section sheets #36 & 37, and the Report of Subsurface Exploration and Geotechnical Engineering have been updated.
- 5. The Project Bid Form has been revised to accommodate these changes.

Please adjust your bid accordingly.

CONTRACTOR'S SIGNATURE

DATE

Printed Name

Company Name

A COPY OF THIS NOTICE SHALL BE STAPLED TO THE BID PROPOSAL AND MUST BE SIGNED ACKNOWLEDGING RECEIPT

Item Number	Item Description	Unit	Quantity	Item Number	Item Description	Unit	Quantity	OF MISSON			
	ROADWAY:				PEDESTRIAN FACILITIES:			JABRETT C.)			
201-20.10	CLEARING AND GRUBBING	ACRE	1.5	404-30.10	TYPE "C" ASPHALTIC CONCRETE	TONS	7	PE-2005005570			
202-20.10		LS	1	608-60.07	CONCRETE SIDEWALK, CURB RAMP (7" THICK)	SY	25.5	- Ming S/ONAL EN INT			
202-22.95	SAWCUT (ANY DEPTH/MATERIAL)	LF	199	608-60.98	TRUNCATED DOMES FOR CURB RAMPS (NEW CONSTRUCTION)	SF	133	DISCIPLINE: CIVIL ENGINEER L LICENSE NO.: 2005005570 EXPIRATION DATE: 12-31-2021			
203-10.00	CLASS "A" EXCAVATION*	CY CY	15000		STRIPING, SIGNING, AND LIGHTING:			DATE PREPARED 10/28/2021			
203-60.00		CY	500	620-99.01	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 8 IN. YELLOW	LF	2339	ROUTE STATE MO			
304-05.04	TYPE 5 AGGREGATE BASE (4" THICK)	SY	6704.9	620-99.02	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 8 IN. WHITE	LF	2169				
405-30.30	TYPE "X" BITUMINOUS CONCRETE (BASE)	TONS	9.2	620-99.03	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 12 IN. WHITE	LF	61	ST. CHARLES			
502-11.08	CONCRETE PAVEMENT (8" NON-REINFORCED)	SY	6264.5	620-99.04	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 24 IN. WHITE	LF	260	CMAQ#4917(602)			
603-10.99	ADJUST UTILITY COVER TO GRADE	EA	1	620-99.05	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 24 IN. YELLOW	LF	180	PROJECT NO.			
604-14.01	AREA INLET, SINGLE, OPEN 1 SIDE, UNTRAPPED	EA	1	620-99.06	PREFORMED THERMOPLASTIC PAVEMENT MARKING STRAIGHT ARROW	EA	1	19STR30 BRIDGE NO.			
604-20.26	ADJUST GRATE INLET TO GRADE	EA	3								
607-01.60	CHAIN LINK FENCE (60")	LF	474	620-99.07	PREFORMED THERMOPLASTIC PAVEMENT MARKING, LEFT/RIGHT ARROW	EA	1				
608-10.00	CONCRETE MEDIAN	SY	460.1				_				
609-10.41	CONCRETE GUTTER, TYPE "A"	LF	78	620-99.08	PREFORMED THERMOPLASTIC PAVEMENT MARKING, COMBINATION STR/LT/RT	EA	5				
609-10.55	CURB AND GUTTER, MOUNTABLE (3")	LF	384	620-99.09	PREFORMED THERMOPLASTIC, PAVEMENT MARKING, BIKE LANE	EA	3				
609-10.99	CONCRETE GUTTER, MODIFIED TYPE "A"	LF	474	620-99.10	PREFORMED THERMOPLASTIC PAVEMENT MARKING, WORD (YIELD)	EA	3				
609-20.11	INTEGRAL CURB (6" HEIGHT AND UNDER)	LF	469	628-00.10	ROADWAY SIGNS (FURNISH AND INSTALL, PERMANENT)	SF	111				
609-60.98	FURNISHING TYPE 3 ROCK DITCH LINER	CY	296	628-00.98	SH-FLAT SHEET	SF	50				
609-60.99	PLACING TYPE 3 ROCK DITCH LINER	CY	296	628-00.99	GROUND MOUNTED SIGN POST	EA	32	DATE 0/25/2			
609-70.00	BEDDING MATERIAL FOR ROCK DITCH LINER	CY	108	901-10.30	LIGHTING POLE, 30 FT, TYPE AT (POWDER COATED BLACK)	EA	10				
612-10.20	MOVEABLE BARRICADES WITH MODEL "B" AMBER FLASHERS	FA	21	901-13.12	LUMINAIRE, LED-B, TENON MOUNT (POWDER COATED BLACK)	EA	10				
	(2 EACH PER BARRICADE)			901-30.02	CONDUIT, 2" RIGID, IN TRENCH	LF	1038	NRLES R			
612-70.20			302	901-30.03	CONDUIT, 3" RIGID, IN TRENCH	LF	207				
616-10.05			392 05	901-30.04	CONDUIT, 4" RIGID, IN TRENCH	LF	15	COADO			
617 20 00			90 EE	901-40.03	CONDUIT, 3" RIGID, PUSHED	LF	188	Y			
617-30.00		LF	55	901-61.10	PULL BOX, PREFORMED CLASS 1	EA	6				
619-00.00		LS	1	901-70.08	CABLE, #8 AWG, 1 CONDUCTOR	LF	3500				
627-40.99		LS	1	901-71.10	POLE & BRACKET CABLE	LF	1020	23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-229 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239 23-239			
703-05.00	GRAFITI PROTECTION SYSTEM		1	901-70.08	WIRE, #8 AWG, BARE NEUTRAL	LF	1750				
703-05.99				901-82.30	POLE FOUNDATION, 30 FT	EA	10				
720-10.00			5894	901-86.12	POWER SUPPLY ASSEMBLY & CONTROLLER, 240 V LTG	EA	1	Earling and a state of the stat			
726-13.12			37	901-99.01	REMOVAL OF EXIST. LIGHTING EQUIPMENT	LS	1	HE PO			
/31-00.48	PRECAST CONCRETE MANHOLE (48")	EA	1	901-99.02	BRACKET ARM, 2 FT, DECORATIVE (POWDER COATED BLACK)	EA	3				
803-10.00	SODDING	SY	3114	901-99.03	PEDESTRIAN LIGHT POLE & FOUNDATION	EA	8				
804-10.00	TOPSOIL	CY	346	901-99.04	PEDESTRIAN LUMINAIRE	EA	11	A A A A			
805-10.00	SEEDING	ACRE	0.4		LANDSCAPING/STREESCAPING:			I I Š Š F P			
806-00.99	SEDIMENT REMOVAL	CY	28.0	840-90.99	LANDSCAPING	LS	1				
806-20.00	PERMANENT EROSION CONTROL BLANKET	SY	250.0								
806-30.01	ROCK DITCH CHECK	EA	26	GROUND				╞╋╝╔╝			
806-50.00	TEMPORARY SEEDING AND MULCHING	ACRE	1.0	STABILIZE	ED EARTH WALL SYSTEMS PAY ITEM.			– –			
806-70.00	SILT FENCE	LF	193								

	CONCRETE MEDIAN										
LOCATION	STATION	STATION	CONCRETE MEDIAN	PIGMENTING AND TEXTURING CONCRETE PAVEMENT AND MEDIAN	REMARKS						
			(SY)	(SY)							
LITTLE HILLS - WEST	202+28.68	203+41.96	263.0	263.0							
LITTLE HILLS - EAST	300+80.86	301+06.20	43.4	43.4							
LITTLE HILLS - EAST	301+16.49	301+71.97	20.7	20.7							
MEL WETTER PARKWAY	59+91.40	60+19.92	33.0	33.0							
MEL WETTER PARKWAY	60+29.97	60+61.31	100.0	100.0							
	TOTAL		460.1	460.1							
	USE		460.1	460.1							

SAWCUT									
LOCATION	STATION	SAWCUT (ANY DEPTH/MATERIAL)	REMARKS						
		LENGTH (LF)							
LITTLE HILLS - WEST	200+00.00	43.0							
LITTLE HILLS - EAST	302+88.48	41.6							
MEL WETTER PARKWAY	59+60.47	54.3							
MEL WETTER PARKWAY	60+08.40	10.5	GREENWAY						
LITTLE HILLS INDUSTRIAL	71+38.88	49.7							
TOTAL		199.1							
USE		199							

ADJUSTMENTS										
LOCATION	STATION	ADJUST GRATE INLET TO GRADE	ADJUST UTILITY COVER TO GRADE	REMARKS						
		EACH (EA)	EACH (EA)							
MEL WETTER PARKWAY	59+92.03	1								
MEL WETTER PARKWAY	60+76.03	1								
LITTLE HILLS INDUSTRIAL	70+53.49	1								
LITTLE HILLS - EAST	300+97.11		1							
	TOTAL	3	1							
	USE	3	1							

MOBILIZATION

LUMP SUM = 1

REMOVAL OF IMPROVEMENTS

LUMP SUM = 1

CONTRACTOR FURNISHED SURVEYING AND STAKING

LUMP SUM = 1

CLEARING AND GRUBBING										
LOCATION	SIDE	AREA	REMARKS							
		(AC)								
LITTLE HILLS EXPRESSWAY	вотн	1.46								
TOTAL		1.46								
USE		1.5								

2 EARTHWORK									
LOCATION	CLASS 'A' EXCAVATION	COMPACTING EMBANKMENT	REMARKS						
	VOLUME (CY)) VOLUME (CY)							
LITTLE HILLS EXPRESSWAY	10300	500							
MSE WALL A	4700								
	> >								
TOTAL	15000	500							
USE	5000	500							
	·								

CONCRETE PAVEMENT										
LOCATION	CONCRETE PAVEMENT (8" NON-REINFORCED)	TYPE 5 AGGREGATE FOR BASE (4" THICK)	PIGMENTING AND TEXTURING CONCRETE PAVEMENT, TRUCK APRON	REMARKS						
	AREA (SY)	AREA (SY)	AREA (SY)							
LITTLE HILLS EXPRESSWAY	6264.5	6507.2	408.4							
TOTAL	6264.5	6507.2	408.4							
USE	6264.5	6507.2	408.4							



					CURB & GUT	ITER				
LOCATION	STATION	STATION	SIDE	INTEGRAL CURB (6" HEIGHT AND UNDER)		CURB AND GUTTER, MOUNTABLE (3")		CONCRETE GUTTER, TYPE "A"		REMARKS
				LENGTH	1 (LF)	LENG	TH (LF)	LENGTH (LF)		REMARKS CENTER ISLAND
LITTLE HILLS EXPRESSWAY	10+00.00	15+78.05	LEFT	320.	.4					CENTER ISLAND
LITTLE HILLS EXPRESSWAY	10+00.00	15+78.05	LEFT			38	33.3			
LITTLE HILLS INDUSTRIAL	70+16.92	70+75.20	LEFT	21.8	8					
LITTLE HILLS INDUSTRIAL	70+19.87	70+75.20	LEFT	61.2	2					
LITTLE HILLS INDUSTRIAL	70+55.06	70+75.20	RIGHT	65.5	5					
LITTLE HILLS - WEST	200+45.57	200+49.59	LEFT					6.3		
LITTLE HILLS - EAST	301+00.65	301+48.04	LEFT					71.4		
		TOTAL		468.	9	38	33.3	77.7		
		USE		469)	3	84	78		
				SIDEV	VALK					
LOCATION	TYPE "C" ASPHALT	IC CONCRETE	CONCRETE SI	DEWALK, CURB RAMP (7" THICK)	TYPE 5 AGGREGATE I	5 AGGREGATE FOR BASE (4" THICK) TRUNCATED DOMES FOR CURB RAMPS (NEW CONSTRUCTION)				

SIDEWALK												
LOCATION	TYPE "C" ASPHALTIC CONCRETE	CONCRETE SIDEWALK, CURB RAMP (7" THICK)	TYPE 5 AGGREGATE FOR BASE (4" THICK)	TRUNCATED DOMES FOR CURB RAMPS (NEW CONSTRUCTION)	RE							
	(TONS)	AREA (SY)	AREA (SY)	AREA (SF)								
LITTLE HILLS EXPRESSWAY	7.0	25.5	197.7	132.6								
TOTAL	7.0	25.5	197.7	132.6								
USE	7.0	25.5	197.7	133								

	STORM SEWER													
LOCATION	STATION	N OFFSET STRUCTURE NUMBER		TO STRUCTURE	PIPE OPENINGS	AREA INLET, SINGLE, OPEN 1 SIDE, UNTRAPPED	PRECAST CONCRETE MANHOLE (48")	12" CLASS III REINFORCED CONRETE PIPE CULVERT						
						EACH (EA)	EACH (EA)	LENGTH (FT)	-					
MEL WETTER PARKWAY	60+21.31	47.04	1-1	1-2	1-12"		1	36.9						
MEL WETTER PARKWAY	60+47.05	77.3	1-2		1-12"	1								
					TOTAL	1	1	37						
					USE	1	1	37						

				<u>2</u> V	VALL				
LOCATION	STATION	STATION	MECHANICALLY STABILIZED EARTH WALL SYSTEMS	CONCRETE GUTTER, MODIFIED TYPE "A"	CHAIN LINK FENCE (60")	GRAFFITI PROTECTION SYSTEM	CONCRETE AND MASONRY PROTECTION	WALL LETTERING AND MOUNTING	WAL SIG
		>	AREA (SF)	LENGTH (LF)	LENGTH (LF)	LUMP SUM (LS)	LUMP SUM (LS)	LUMP SUM (LS)	LU
LITTLE HILLS EXPRESSWAY	10+00.00	14+71.70	5894.1	474.0	474.0	1	1	1	
		(К					
TOTAL		5	5894.1	474.0	474.0	1	1	1	
USE			5894	474	474	1	1	1	
			h						





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Certific Expiration

		1	1	TEMPORA	ARY TF	RAFFIC CONTROL	I			
LOCATION	SIGN	SIZE	QUANTITY	CONSTRUCTION SIGNS		DESCRIPTION	MOVEABLE BA "B" AMBER F B	RRICADES WI LASHERS (2 EA ARRICADE)	TH MODEL ACH PER	CHA (TF
	(LF)	(IN)	(EA)	(SF)				(EA)		
LITTLE HILLS EXPRESSV	VAY W020-1	48X48	2	32		ROAD WORK AHEAD				
LITTLE HILLS EXPRESSV	VAY G020-2	48X24	2	16		END ROAD WORK				
LITTLE HILLS EXPRESSV	VAY W01-4L	48X48	1	16		REVERSE CURVE (LEFT)				
LITTLE HILLS EXPRESSV	VAY W01-4R	48X48	1	16		REVERSE CURVE (RIGHT)				
	VAY W021-5	48X48	2	32		SHOULDER WORK AHEAD				
	VAY W020-4	48X48				ONE LANE ROAD AHEAD				
LITTLE HILLS EXPRESSV	VAY W020-7a	48X48	0	0		FLAGGER WITH FLAGS				
	VAY W5-1	48X48	1	16		ROAD NARROWS				
LITTLE HILLS EXPRESSV	VAY R11-2	48X30		50		ROAD CLOSED				
LITTLE HILLS EXPRESSV	VAY M04-9L	30X24	5	25		DETOUR (LEFT)				
LITTLE HILLS EXPRESSV	VAY M04-9R	30X24	5	25		DETOUR (RIGHT)				
LITTLE HILLS EXPRESSV	VAY M04-8	24X12	4	8		DETOUR				
LITTLE HILLS EXPRESSV	VAY M6-3	24X12	4	8		STRAIGHT ARROW				
LITTLE HILLS EXPRESSV	VAY M04-8a	24X18	1	3		END DETOUR				
LITTLE HILLS EXPRESSV	VAY W020-3	48X48	1	16		ROAD CLOSED AHEAD				
LITTLE HILLS EXPRESSV	VAY R11-3A	60X30	2	25		LOCAL TRAFFIC AHEAD				
LITTLE HILLS EXPRESSV	VAY SPECIAL SIGN	30X18	15	56		FIFTH ST				
LITTLE HILLS EXPRESSV	VAY SPECIAL SIGN	48x36	2	24		PROJECT INDENTIFICATION - CITY				
	VAYSPECIAL SIGN		200	24		PROJECT INDENTIFICATION - COUNTY				
					<u> </u>			21		
	VAY	<u>h</u>			\mathcal{I}		$+\cdots$			
LITTLE HILLS EXPRESSV	VAY									
				2			2	~~~~		
			TOTAL	392.0				21		
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	SOD	DING								 IT
					\rightarrow		, 			
LOCATION	SODDING	-	TOPSOIL	REMARKS		LOCATION		BITU	MINOUS PA PG64-2	/EMEN1 2 (BASE
	AREA (SY)	V	OLUME (CY)							
LITTLE HILLS EXPRESSWAY	3113.5		345.9			LITTLE HILLS EXPRESSWAY	226.7	0.5	4.2	
	0440 5		245.0		<u> </u>					1
	3113.5		345.9		$ \langle \rangle $	TOTAL				
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10/28/2021









GENERAL NOTES:

1) DO NOT SCALE DRAWING. FOLLOW DIMENSIONS.

2) ALL SIGNING SHALL BE IN ACCORDANCE WITH THE CURRENT EDITION OF THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES.

3) NO DIRECT PAYMENT WILL BE MADE FOR RELOCATION OF TCP SIGNS AND DEVICES.

4) ANY EXISTING SIGNS THAT CONFLICT WITH TEMPORARY TRAFFIC CONTROL SHALL BE COVERED OR REMOVED.

5) ALL TRAFFIC CONTROL ITEMS WHICH ARE NOT INCLUDED IN THE PAY ITEMS ARE TO BE CONSIDERED INCIDENTAL.

6) CONTRACTOR SHALL MAINTAIN TEMPORARY STRIPING DURING CONSTRUCTION.









10/28/2021











10/28/2021





General Notes: Design Specifications:

2002 AASHTD LFD (17th Ed.) Standard Specifications (Section 5, ASD Design) Selsmic Performance Category D Acceleration Coefficient = _186

Design Loading:

 $\phi_{\!\!\!D}$ = 20° for on-site soils and 35° for crushed stone and Unit weight, = 120 pcf (on-site soil) and 110 pcf (crushed stone) for retained backfill material to be retained by the mechanically stabilized earth wall system. $\phi_{\mathcal{F}} = 2\Omega^{\circ}$ for unimproved foundation ground where wall is to bear.

Actual $\phi_{\mathcal{F}} \geq 34^\circ$ for the select granular backfill (reinforced backfill and wedge area backfill) for structural systems.

Design ϕ_r = 34° for the select granular backfill (reinforced backfill) only for structural systems.

The allowable bearing pressure for unimproved foundation ground 1.50 ksf.

The maximum applied bearing pressure for the controlling design case at the foundation level shall be shown on the manufacturer's design plans where the maximum applied bearing pressure \leq allowable bearing pressure. For selsmic design the maximum applied bearing pressure \leq two times allowable bearing pressure.

Factor of safety shall be 2.0 for overturning and 1.5 for sliding. For seismic design the factor of safety shall be 1.5 for overturning and 1.1 for sliding.

Use default values for the pullout friction factor, F*, in accordance with AASHTO figure 5.8.5.24. For approved steel strips not shown in AASHTO figure 5.8.5.24. use F* ≤ 2.0 at zero depth and F* ≤ 1 an ϕ_- at 20 feet depth and ϕ_- design = 34°. F* values shall be shown on the manufacturer's design plans.

Design Unit Stresses:

All concrete for leveling pad and coping shall be Class B or B-1 with f'c = 4000 psi.

Miscellaneous: The MSE wall system shall be built vertical.

The MSE wall system shall be built in accordance with Sec 720. The MSE wall system shall be a large block wall system.

Panel and coping (or capstone) reinforcement shall be epoxy coated.

A filter cloth meeting the requirements for a Separation Geotextile material shall be placed between the select granular backfill for structural systems and the backfill being retained by the mechanically stabilized earth wall system.

Coping shall be required on this structure. Bond breaker (roofing felt or other approved alternate) between wall panel and coping required if coping is cast in place.

The top and bottom elevations are given for a vertical wall. If a fence is built on an extended gutter, then the height of the wall shall be adjusted further.

The contractor shall be solely responsible to coordinate construction of the wall with readway construction and ensure that the readway construction, resulting or existing obstructions, shall not impact the construction or performance of the wall. Soil reinforcement shall be designed and placed to avoid damage by pile driving, guardrail post installation, utility and sign foundations. (See Roadway plans.)

Minimum 18" wide Geotextile strips shall be centered at vertical and horizontal joints of panel. Geotextile material shall be adhered to back face of panel using an adhesive compound supplied by the manufacturer.

Aluminized soil reinforcement shall have edges coated with coating material per manufacturer.

If rock is encountered in the proposed reinforced backfill area or wedge area of the MSE wall before or during excavation, the contractor shall immediately cease excavating and notify the engineer.

Concrete and Masonry Protection shall be applied to exposed concrete face of proposed retaining wall.

Concrete and Masonry Protection Graffiti Protection System

10+75.00 EL 548.76 +00.00 548.81 <u>10+50.00</u> EL 548.63 +25.00 11+50.00 EL 548.56 8 <u>12+00.00</u> EL 548.31 12+25.00 EL 548.19 <u>12+50.00</u> EL 548.06 <u>12+75.00</u> EL 547.55 11+75.(EL 548.2 10+25.00 EL 546.96 13+00.00 EL 546.80 . 13+25.00 EL 546.05 Graffiti Protection System shall be applied to proposed retaining wall to a height of STA. 13+50.00 EL 545.30 10+00.00 EL 544.69 12' above finished grade. STA. Ţ. Ground remediation and any required excavation are to be considered incidental VPI 10+92.99 EL 548.85 to Mechanically Stabilized Earth Wall 10+43.08 L 548.60 Systems pay item. I 12+59.53 EL 548.02 Top of Coping VPI 13+50.00 EL 545.30 e Proposed Grade VP I STA. 10+00.00 EL 542.15 STA. 10+25.00 EL 540.99 Estimated limit of STA. 10+50.00 EL 539.85 STA. 10+45.16 EL 540.06 Graffiti Protection System STA. 10+75.00 EL 538.79 STA. 10+95.25 EL 537.92 STA. 11+00.00 EL 537.73 STA. 11+25.00 EL 536.73 STA. 11+45.33 EL 535.92 STA. 11+50.00 EL 535.75 STA. 11+75.00 EL 534.83 STA. 12+00.00 EL 533.96 STA. 11+95.41 EL 534.08 STA. 12+75.00 EL 532.17 STA. 12+83.98 EL 531.96 STA. 12+96.16 STA. 12+96.16 STA. 13+00.00 STA. 13+00.00 STA. 12+28.29 EL 533.25 STA. 12+25.00 EL 533.33 STA. 12+50.00 EL 532.75 STA. 12+64.31 EL 532.42 STA. 13+25.00 EL 530.50 STA. 13+54.05 EL 529.46 STA. 13+38.80 EL 530.05 STA. 13+50.00 EL 529.62 * Wall contractor shall show the following items on the design drawings and/or on the fabricator shop drawings. Leveling pad horizontal.
 Leveling pad length and step elevations shall be based on wall monufacturer's recommendation. Top of leveling pad elevations shall not be higher than theoretical top of leveling pad elevations shown on these plans. DEVELOPED ELEVATION Estimated Quantities
 Total

 sq. foot
 5894

 lump sum
 1

 lump sum
 1
 ltem Mechanically Stabilized Earth Wall Systems

Indicates location of borings. Notice and Disclaimer Regarding Boring Log Data

The locations of all subsurface borings for this structure are shown on the plan sheet(s) for this on the plan sheet(s) for this structure. The boring data for all locations indicated, as well as any other boring logs or other factual records of subsurface data and investigations performed by the department for the design of the project, are shown on Sheet(s) No. __ and may be included in the Electronic Bridge Deliverables. They will also be available from the Project Contact upon written request. No greater significance or weight should be given to the boring data depicted on the plan sheets than is given to the subsurface data available from the district or elsewhere. district or elsewhere.

The Commission does not represent or warrant that any such boring data accurately depicts the conditions to be encountered in constructing this be encountered in constructing this project. A contractor assumes all risks it may encounter in basing its bid prices, time or schedule of performance on the boring data depicted here or those available from the district, or on any other documentation not expressly warranted, which the contractor may obtain from the formission obtain from the Commission.

DEVELOPED ELEVATION

PLAN

-Existing Ground

Concrete Leveling pad not shown for clarity. *

Note: This drawing is not to scale. Follow dimensions.





NAT DIS	ME CIPLE					JASI JASI	ERR 25021	AND DATED
	10/28/2021 ROUTE STATE MO DISTRICT SHEET NO. 25							
c	COUNTY ST. CHARLES JOB NO. CMAQ#4917(602) CONTRACT ID. PROJECT NO. 19STR30 BRIDGE NO.							ET IT HAS BEEN ELECTRONIC
DESCRIPTION	ADDENDUM 2							IF A SEAL IS DRESENT ON THIS SHE
DATE	10/25/21							





LITTLE HILLS EXPRESSWAY MSE WALL DETAILS SHEET 2 OF 3

***** Select granular backfill shall extend a minimum of 12" beyond the end of all soil reinforcement. Where the angle, 8, between the retained backfill excavation/fill line and the horizontal is less than 90°, the wedge area backfill between 0 and 90° shall be filled with select granular backfill for structural systems meeting the requirements of Section 1010.

- For $(45^\circ + \phi_5/3) < \theta \le 90^\circ$, properties for retained backfill shall

- For $\theta \leq (45^\circ + \phi_b/3)$, contractor shall have the option to use select granular backfill, ϕ_{μ} , or better aggregate material, $\phi_{\mu\nu}$ for active force computations in the wedge area backfill. For active force computations, the angle of internal friction for wedge area backfill material, ϕ_r or ϕ_w , shall be limited to 34° unless determined otherwise in accordance with Section 1010. If ϕ_{μ} or $\phi_{\mu} > 34^{\circ}$ is desired for wedge area backfill then test report shall be submitted with manufacturer's design plans. ϕ_r or ϕ_w shall not be greater than 40° for computations. Final configuration of this option shall be sent to Geotechnical Section for a new overall global stability analysis. Design ϕ_w shall be shown on manufacturer's plans if used.

The slope excavation line shall be benched and separation geotextile shall be placed between the retained backfill and either select granular backfill or better aggregate material, and between the select granular backfill and

Show range of acceptable theta (B) angle on shop drawings which must be consistent with design computations and proposed construction of wall. Show active force computation properties on shop drawings and in design computations. Coordination between wall designer (manufacturer) and





3.0 Work Hour Restrictions.

3.1 There are three major summer holiday periods: Memorial Day, Independence Day, and Labor Day. All lanes shall be scheduled to be open to traffic during these holiday periods, from 12:00 noon on the last working day preceding the holiday until 9:00 a.m. on the first working day subsequent to the holiday. Normal daytime traffic operations shall be considered 8:00 a.m. to 4:00 p.m to avoid peak travel times.

4.0 Traffic Control Plan.

4.1 Traffic Control sign, cones & other devices to be provided by the contractor shall comply with the Manual of Uniform Traffic Control Devices (MUTCD), latest edition. The contractor shall have day to day responsibility for traffic control in work zone areas, and shall provide additional traffic control measures as they deem appropriate to provide for safe traffic and pedestrian control and related construction operations.

4.2 The contractor will ensure that two-way travel will be maintained on Little Hills Expressway during construction. Mel Wetter Parkway and Little Hills Industrial Boulevard will be closed for a short duration during construction. Signed detours will be set up during the road closures of Mel Wetter Parkway and Little Hills Industrial Boulevard. Below is a summary of the construction phasing for the project:

4.2.1 Phase 1: The northern portion of the roundabout and the new road north of existing Little Hills Expressway will be constructed. Two lanes and two-way traffic will be maintained on Little Hills Expressway in this phase.

4.2.2 Phase 2: Connections of the new roundabout to Little Hills Expressway will be constructed. Westbound traffic will be moved onto new roundabout. Eastbound traffic will continue to use existing Little Hills Expressway. Mel Wetter Parkway and Little Hills Industrial Boulevard will have access to eastbound Little Hills Expressway only.

4.2.3 Phase 3: The southern portion of the roundabout will be constructed, including the connections to Mel Wetter Parkway and Little Hills Industrial Boulevard. Two-way traffic will be maintained on the newly constructed north side of the roundabout. Mel Wetter Parkway and Little Hills Industrial Boulevard shall be closed during construction of Phase 3. The closure of Mel Wetter Parkway and Little Hills Industrial Boulevard shall be limited to 60 calendar days at which point the contractor is subject to liquidated damages in the amount of \$1,100/day.

5.0 Greenway/Trail Access. Access to the trail crossing across Mel Wetter Parkway shall be provided whenever feasible. The crossing shall be returned to ADA compliance in a reasonably attainable manner as agreed upon by the City and the contractor.

6.0 Basis of Payment. No direct payment will be made to the contractor to recover the cost of equipment, labor, materials or time required to fulfill the above provisions, unless specified elsewhere in the contract document.

Q. <u>ROADWAY SIGNS/SIGN POSTS</u>

1.0 Description. This work shall consist of furnishing and installing signs as shown on the plans. All signs shall be in accordance with the Manual on Uniform Traffic Control Devices (MUTCD). Any signs not detailed on the plans shall be in accordance with Standard Highway Signs by the U.S. Department of Transportation, Federal Highway Administration.

1.1 This work shall include all labor and equipment necessary to erect Roadway Signs and Ground Mounted Sign Posts.

1.2 Where called for on the Project Drawings, in the details, or as instructed by the Project Engineer, install appropriate Roadway Signs and Ground Mounted Sign Posts as directed in the plans.

1.3 Road signs shall be installed according to the AASHTO MUTCD. Road signs shall be installed on a single black square tube post with a breakaway assembly, where necessary.

2.0 Materials. Material shall conform to the Missouri Standard Specifications for Highway Construction, Division 1000 Materials Details.

3.0 Method of Measurement.

3.1 Measurement for these work items shall be as indicated below:

Roadway Signs (Furnish and Install, Permanent), measured per Square Foot Ground Mounted Sign Posts, measured per Each

4.0 Basis of Payment

4.1 Payment for this work shall be as follows:

Roadway Signs (Furnish and Install, Permanent), measured per Square Foot Ground Mounted Sign Posts, measured per Each

	Project Bid Form Little Hills Expressway and Mel Wetter Parkway Intersection Improvements CMA0#4917(602) City of Science Minerary							
Item Number	Item Description	Unit	Quantity	Unit Price	Total			
	ROADWAY:							
201-20.10	CLEARING AND GRUBBING	ACRE	1.5					
202-20.10	REMOVAL OF IMPROVEMENTS	LS	1					
202-22.95	SAWCUT (ANY DEPTH/MATERIAL)	LF	199					
203-10.00	CLASS "A" EXCAVATION	CY	15000					
203-60.00	COMPACTING EMBANKMENT	CY	500					
304-05.04	TYPE 5 AGGREGATE BASE (4" THICK)	SY	6704.9					
405-30.30	TYPE "X" BITUMINOUS CONCRETE (BASE)	TONS	9.2					
502-11.08	CONCRETE PAVEMENT (8" NON-REINFORCED)	SY	6264.5					
603-10.99	ADJUST UTILITY COVER TO GRADE	EA	1					
604-14.01	AREA INLET, SINGLE, OPEN 1 SIDE, UNTRAPPED	EA	1					
604-20.26	ADJUST GRATE INLET TO GRADE	EA	3					
607-01.60	CHAIN LINK FENCE (60")	LF	474					
608-10.00	CONCRETE MEDIAN	SY	460.1					
609-10.41	CONCRETE GUTTER, TYPE "A"	LF	78					
609-10.55	CURB AND GUTTER, MOUNTABLE (3")	LF	384					
609-10.99	CONCRETE GUTTER, MODIFIED TYPE "A"	LF	474					
609-20.11	INTEGRAL CURB (6" HEIGHT AND UNDER)	LF	469					
609-60.98	FURNISHING TYPE 3 ROCK DITCH LINER	CY	296					
609-60.99	PLACING TYPE 3 ROCK DITCH LINER	СҮ	296					
609-70.00	BEDDING MATERIAL FOR ROCK DITCH LINER	CY	108					
612-10.20	MOVEABLE BARRICADES WITH MODEL "B" AMBER FLASHERS(2 EACH PER BARRICADE	EA	21					
612-70.20	CHANGEABLE MESSAGE BOARD (NOISELESS), RENTAL	EA	3					
616-10.05	CONSTRUCTION SIGNS	SF	392					
616-10.25	CHANNELIZER (TRIM LINE)	EA	95					
617-30.00	PERMANENT CONCRETE MEDIAN BARRIER, TYPE "D"	LF	55					
619-00.00	MOBILIZATION	LS	1					
627-40.99	CONTRACTOR FURNISHED SURVEYING AND STAKING	LS	1					
703-05.00	GRAFITTI PROTECTION SYSTEM	LS	1					
703-05.99	CONCRETE AND MASONRY PROTECTION SYSTEM	LS	1					
720-10.00	MECHANICALLY STABILIZED EARTH WALL SYSTEMS	SF	5894					
726-13.12	12" CLASS III REINFORCED CONCRETE PIPE CULVERT	LF	37					
731-00.48	PRECAST CONCRETE MANHOLE (48")	EA	1					
803-10.00	SODDING	SY	3114					
804-10.00	TOPSOIL	CY	346					
	1	I	1	1				









Item Number	Item Description	Unit	Quantity	Unit Price	Total
805-10.00	SEEDING	ACRE	0.4		
806-00.99	SEDIMENT REMOVAL	СҮ	28		
806-20.00	PERMANENT EROSION CONTROL BLANKET	SY	250		
806-30.01	ROCK DITCH CHECK	EA	26		
806-50.00	TEMPORARY SEEDING AND MULCHING	ACRE	1		
806-70.00	SILT FENCE	LF	193		
			1	SUBTOTAL	
Item Number	Item Description	Unit	Quantity	Unit Price	Total
	PEDESTRIAN FACILITIES:				
404-30.10	TYPE "C" ASPHALTIC CONCRETE	TONS	7		
608-60.07	CONCRETE SIDEWALK, CURB RAMP (7" THICK)	SY	25.5		
608-60.98	TRUNCATED DOMES FOR CURB RAMPS (NEW CONSTRUCTION)	SF	133		
				SUBTOTAL	
	STRIPING, SIGNING, AND LIGHTING:				
620-99.01	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 8 IN. YELLOW	LF	2339		
620-99.02	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 8 IN. WHITE	LF	2169		
620-99.03	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 12 IN. WHITE	LF	61		
620-99.04	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 24 IN. WHITE	LF	260		
620-99.05	PREFORMED THERMOPLASTIC PAVEMENT MARKING, 24 IN. YELLOW	LF	180		
620-99.06	PREFORMED THERMOPLASTIC PAVEMENT MARKING, STRAIGHT ARROW	EA	1		
620-99.07	PREFORMED THERMOPLASTIC PAVEMENT MARKING, LEFT/RIGHT ARROW	EA	1		
620-99.08	PREFORMED THERMOPLASTIC PAVEMENT MARKING, COMBINATION STR/LT/RT	EA	5		
620-99.09	PREFORMED THERMOPLASTIC, PAVEMENT MARKING, BIKE LANE	EA	3		
620-99.10	PREFORMED THERMOPLASTIC PAVEMENT MARKING, WORD (YIELD)	EA	3		
628-00.10	ROADWAY SIGNS (FURNISH AND INSTALL, PERMANENT)	SF	111		
628-00.98	SH-FLAT SHEET	SF	50		
628-00.99	GROUND MOUNTED SIGN POST	EA	32		
901-10.30	LIGHTING POLE, 30 FT, TYPE AT (POWDER COATED BLACK)	EA	10		
901-13.12	LUMINAIRE, LED-B, TENON MOUNT (POWDER COATED BLACK)	EA	10		
901-30.02	CONDUIT, 2" RIGID, IN TRENCH	LF	1038		
901-30.03	CONDUIT, 3" RIGID, IN TRENCH	LF	207		
901-30.04	CONDUIT, 4" RIGID, IN TRENCH	LF	15		
901-40.03	CONDUIT, 3" RIGID, PUSHED	LF	188		
901-61.10	PULL BOX, PREFORMED CLASS 1	EA	6		
901-70.08	CABLE, #8 AWG, 1 CONDUCTOR	LF	3500		
901-71.10	POLE & BRACKET CABLE	LF	1020		
901-70.08	WIRE, #8 AWG, BARE NEUTRAL	LF	1750		

Item Number	Item Description	Unit	Quantity	Unit Price	Total
901-82.30	POLE FOUNDATION, 30 FT	EA	10		
901-86.12	POWER SUPPLY ASSEMBLY & CONTROLLER, 240 V LTG	EA	1		
901-99.01	REMOVAL OF EXIST. LIGHTING EQUIPMENT	LS	1		
901-99.02	BRACKET ARM, 2 FT, DECORATIVE (POWDER COATED BLACK)	EA	3		
901-99.03	PEDESTRIAN LIGHT POLE & FOUNDATION	EA	8		
901-99.04	PEDESTRIAN LUMINAIRE	EA	11		
		SUBTOTAL		SUBTOTAL	
	LANDSCAPING/STREESCAPING:				
840-90.99	LANDSCAPING	LS	1		
		SUBTOTAL		SUBTOTAL	
		PARTICIPATING COSTS TOTAL			

	Non-Participating Construction Costs								
Item Number	Item Description	Unit	Quantity	Unit Price	Total				
	ROADWAY:								
608-99.06	PIGMENTING AND TEXTURING CONCRETE PAVEMENT AND MEDIAN	SY	868.5						
720-10.99	WALL LETTERING AND MOUNTING ACCESSORIES	LS	1						
901-99.05	WALL MOUNTED SIGN LIGHTING SYSTEM	LS	1						
				SUBTOTAL					
	WATER MAIN:								
1	12" PVC C900 DR14 (OPEN CUT) (INCLUDING EXCAVATION AND BEDDING)	LF	2253						
2	12" DIP RESTRAINED JOINT (HORIZONTAL DIRECTIONAL DRILL) (INCLUDING EXCAVATIO	LF	120						
3	6" DIP RESTRAINED JOINT WATER MAIN (OPEN CUT) (INCLUDING EXCAVATION AND BE	LF	94						
4	6" PVC C900 DR14 (INCLUDING EXCAVATION AND BEDDING)	LF	100						
5	6" DIP WATER MAIN	LF	148						
6	6" DIP FITTINGS	EA	3						
7	12" DIP FITTINGS	EA	14						
8	12" GATE VALVE	EA	3						
9	6" GATE VALVE	EA	3						
10	HYDRANT ASSEMBLY (INCL. EXCAVATION, BEDDING, VALVE, TEE, PIPE SPOOL)	EA	5						
11	10" TAPPING SLEEVE & VALVE	EA	1						
12	CONNECTION TO EXISTING 12" MAIN	EA	1						
13	CONNECTION TO EXISTING 6" MAIN	EA	3						
14	GRANULAR BACKFILL	CY	609						

Item Number	Item Description	Unit	Quantity	Unit Price	Total
15	ASPHALT PAVEMENT REMOVAL & REPLACEMENT	SY	84		
16	CONCRETE REMOVAL & REPLACEMENT	SY	154		
17	CONCRETE REMOVAL & REPLACE WITH TEMPORARY ASPHALT	SY	38		
18	ASPHALT PAVEMENT REMOVAL ONLY	SY	190		
19	TREE CLEARING	LS	1		
20	TRAFFIC CONTROL	LS	1		
				SUBTOTAL	
			NON-PART	ICIPATING COSTS TOTAL	



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October 28, 2021

Mr. Jonathan R. Loos, P.E. Horner & Shifrin, Inc. 401 S. 18th Street, Suite 400 St. Louis, MO 63103

SUBJECT:Report of Subsurface Exploration and Geotechnical EngineeringEvaluation for Little Hills Expressway, St. Charles, Missouri rev 1

Dear Mr. Loos:

ABNA Engineering, Inc., has completed the authorized Subsurface Exploration and Geotechnical Engineering Evaluation of the subject project. Our work was done in general accordance with the Professional Service Agreement dated July 15, 2019.

The purpose of our work was to determine the general subsurface conditions at specific soil test boring locations and to gather data on which to base comments relative to the selection of foundation types for the proposed structure at the site and assess the existing pavement at roughly third points within the project. This report outlines the exploration procedures used, exhibits the data obtained, and presents our evaluation and recommendations relative to the outlined geotechnical engineering aspects of the project.

We appreciate the opportunity to work with you on this project. Please contact our office if we can be of further assistance.

Respectfully submitted, **ABNA Engineering, Inc.**



Geotechnical Manager

Civil · Structural · Testing & Inspection · CM · Surveying · GIS · Planning

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1 SCOPE OF WORK

Our work was performed in general accordance with the Professional Service Agreement dated July 15, 2019. Authorization to proceed was issued by Horner & Shifrin, Inc. Our scope of work consisted of the following:

- 1. Site reconnaissance and boring layout by a staff engineer/surveyor.
- 2. Obtain existing utility information through coordination with utility companies and utility locate service.
- 3. Provide maintenance of traffic per MUTCD guidelines.
- 4. Subsurface Exploration consisting of four (4) soil test borings at the proposed retaining wall location and three (3) test borings along the alignment of the new water main with samples and penetration tests at regular intervals.
- 5. Laboratory soil classification testing on selected soil samples obtained from the soil borings and preparation of the borehole logs.
- 6. Prepare a letter report addressing the findings of the subsurface investigation and geotechnical recommendations as it relates to construction of the proposed gravity block or Mechanically Stabilized Earth (MSE) retaining wall.

2 SITE AND PROJECT DESCRIPTION

The subject site is located within the City of St. Charles, Saint Charles County, Missouri. The subject site lies north east of Route 370 consists of Little Hills Expressway and the Mel Wetter Parkway Roundabout.

The topography of the subject site was observed to be generally sloping from an elevation of 556 ft in the west to 458 ft at the east end of the site with 15 to 20 foot high slopes from street level north of the Little Hills Expressway to the base of the proposed retaining wall. The exposed surfaces were generally covered with wooded vegetation. Figures 1 through 2 show the site in visual detail.

It is our understanding that the proposed project will involve the design of a roundabout capable of accommodating future Route 370 ramps at the intersection of Mel Wetter Parkway and Little Hills Expressway. In the interim, the roundabout will optimize traffic currently experiencing significant traffic delays and experiencing an increase in traffic volumes due to new developments. The project will also consist of a new retaining wall, ADA compliant changes to Boschert Greenway, and a new water main along Little Hills Expressway.

3 SITE GEOLOGY

Published geologic literature (USDA Web Soil Survey and Geologic Map of Missouri) indicates that the site is underlain by silty clay and the bedrock unit is the Mississippian age St. Louis limestone formation. Estimated depth to bedrock at the east end of the project site is approximately 41.5 feet. The soil overburden within the general site vicinity consists of the Menfro silt loam present on 20 to 45 percent slopes. These soil deposits can form on slopes and are well drained silt loams to silty clay loams.

4 SEISMIC

The New Madrid fault zone, which is the primary region of seismic activity for the mid-continental region, is located approximately 150 miles south of the St. Louis area in the southeast corner of Missouri. The strongest recorded earthquakes resulting from this fault zone occurred in December, 1811 through February, 1812, with three principal earthquakes of estimated Intensity XI on the Modified Mercalli Scale.

A secondary source of seismic activity is the St. Genevieve fault zone, which extends northwest/southeast from southwestern Illinois towards St. Genevieve County, Missouri. This fault zone's northern terminus is located within 50 miles of the St. Louis area. Several seismic events of body wave magnitude (mb) 4.5 to 5.8 have been recorded near this fault zone.

5 FIELD EXPLORATION AND LABORATORY TESTING

On August 14 and 17, 2020, ABNA Engineering, Inc. conducted a subsurface exploration consisting of seven (7) soil borings: four (4) at the proposed retaining wall location and three (3) at the proposed new water main. The soil borings are designated as B-01 through B-04. Borings B-01 to B-04 were completed up slope of the roadway along the proposed retaining wall and borings B-05 to B07 were completed at the roadway level along the proposed new water main. Borings B-01 through B-04 were completed to a depth of approximately the existing road elevation. This configuration was utilized to obtain soil samples to provide data for global stability analysis. Borings B-05 was drilled to establish the depth to bedrock and collect a rock sample. Borings B-06 to B-07 were drilled to obtain soil samples and data in the footprint of the proposed new water main. The field investigation was directed by a geotechnical engineer/geologist from ABNA who also classified and collected the soil and rock samples.

In addition to the field exploration, a geotechnical laboratory testing program was conducted to determine additional engineering characteristics of selected soil samples obtained from the soil borings and to test the compressive strength of the rock sample. The results of the individual tests are indicated on the Logs of Boring in Appendix B.

6 SUBSURFACE CONDITIONS

Details of the subsurface conditions encountered by the borings are shown on the Logs of Boring located in Appendix B. The general subsurface conditions encountered on the slopes consisted primarily of brown and gray lean silty clays and loess. Auger refusal was only encountered during boring B-05. Groundwater was not observed during the exploration. The presence or absence of groundwater during drilling does not necessarily mean that groundwater will be present or absent at that location at other times. The results of the Atterberg Limits laboratory tests confirmed the designation of low plasticity lean clay (CL) for 3 samples tested and silt (ML) for one sample.

Conditions represented by the borings should be considered applicable only at the boring locations on the dates shown. It should be assumed that the reported conditions might be different at other locations or at other times.

7 FOUNDATION DESIGN AND CONSTRUCTION RECOMMENDATIONS

7.1 Geotechnical Consideration

Based on our analysis, the new *MSE wall* structure can be supported on a footing foundation system bearing within the soil. Recommendations regarding the design and construction of the foundation are provided below.

7.2 Foundation – Retaining Wall

Below-grade walls required at this site are assumed to include a retaining wall designed to accommodate surface grade changes on the north side of Little Hills Expressway. The maximum toe pressure for below-grade walls should not exceed the bearing pressure of 1,500 pounds per square foot (psf). *Retaining walls designed with a bearing pressure exceeding 1,500 pounds per square foot will need to incorporate some form of ground bearing modification system and/or foundation improvement*. Retaining walls may be designed with an allowable coefficient of friction between the base of the *wall* and the soil subgrade of 0.3 *and between the base of the wall and the porous granular (figure 3) of 0.45*.

Below-grade walls should also be designed to withstand lateral earth pressures caused by the weight of the backfill, including slopes behind the walls; and any surcharge, such as adjacent loads. We recommend the equivalent fluid unit weights tabulated below for lateral earth pressures be used in the design of below-grade walls. The indicated values assume that positive drainage is provided to prevent buildup of hydrostatic pressure. Expansive clay soils should not be used to backfill the wall excavations. Values for granular material should only be used if the granular backfill extends upwards and outwards the full height of the wall at a slope of 45 degrees or flatter from its base. In this case, exterior granular backfill should be capped with approximately 2 feet

of cohesive soil to reduce the potential for surface water infiltration into the granular backfill. With clean granular backfill, filter fabric, such as Mirafi 140N, should be placed along the interface between the soil and granular backfill to reduce the potential for infiltration of the soil into the granular material.

BACKFILL MATERIAL	ON-SITE SOIL	CRUSHED STONE
At-Rest Equivalent Fluid Pressure	80 pcf	50 pcf
Active Equivalent Fluid Pressure	60 pcf	30 pcf
Soil Unit Weight	120 pcf	110 pcf (Crushed Stone)
Soil Angle of Internal Friction	20°	35 °
Assumed Surcharge Condition	None	None
Slope Profile	Horizontal	Horizontal
Drainage Condition	Fully Drained (No	Fully Drained (No
	hydrostatic Pressure	hydrostatic Pressure)

Lateral Earth Pressure Parameters

We recommend that all below-grade walls be provided with a drainage system. A minimum 4inch diameter, perforated drainpipe should be used, and placed at foundation level. Granular drainage material, consisting of 1-inch clean crushed rock, classified as GP by ASTM D 2487, with less than 5 percent of the rock passing the No. 200 sieve, should be placed a minimum of 6 inches in all directions around the drainage pipe. Synthetic filter fabric, such as Mirafi 140N or equivalent, should encapsulate the drainpipe and granular drainage material. The pipe should be sloped to drain by gravity or through weepholes located on approximately 10-foot centers for above-grade retaining walls. Alternately, drainage can be provided directly through the weepholes without a drain pipe, provided that filter fabric is used or other measures are taken to prevent the granular backfill from migrating out through the weepholes.

7.3 Footing Foundation Construction Considerations

Footing excavations should be free of water, loose soil, and debris if and when concrete is placed. Concrete should be placed soon after excavating to reduce bearing material disturbance.

7.4 Design Recommendation for Retaining Wall Footing Bearing on Soil

DESCRIPTION	Design Value
Net allowable bearing pressure ¹	$1,500 \text{ pounds/ft}^2$
<i>Minimum embedment (below lowest exterior grade)</i> ²	30 inches

 The net allowable bearing pressure is the pressure in excess of the minimum surrounding overburden pressure at the footing base elevation for footings founded in soil. Footing excavation should be free of loose and disturbed material, debris, and water when concrete is placed. 1st two feet shall be omitted for passive pressure.
 Minimum depth will help provide frost protection.

7.5 Spread Footings Bearing on Controlled Engineering Fill Construction Considerations

This approach involves over-excavating the existing soil and replacing the over-excavated areas with controlled engineered fill as a way of increasing the allowable maximum bearing capacity. Engineered fill should be free of organic and other deleterious material. The fill should consist of *crushed stone*. The fill should be placed in lifts not exceeding eight inches of loose measure and compacted to 95% of the soil's maximum dry density as determined by the Standard Proctor Compaction Test (ASTM D698).

The retaining wall structure can be supported on a system of footings, *that includes the entire length of the select backfill soil mass for MSE walls, and* derives their support from newly placed controlled engineered fill *(figure 3)*. Footings bearing on controlled engineered fill should be dimensioned for an allowable maximum bearing capacity (bearing capacity in excess of adjacent overburden) of 2,500 pounds per square foot (PSF).



NOT TO SCALE (See plans for actual wall configuration.)

* Depth of porous granular is only at the 16 ft wall maximum height provided in the updated wall sheet plan profiles.

Figure 3 - Controlled Engineered Fill

The footing bearing surfaces should be observed by a geotechnical engineer from ABNA to confirm that the exposed bearing surface complies with the design bearing pressure. Based on the field observation, if localized soft zones are identified, they should be undercut and replaced with controlled engineered fill, crushed stone, or lean concrete. If clean stone is used as backfill material, the clean stone should be enclosed in geotextile fabric to prevent adjacent fine-grained material from migrating into the clean stone.

Soil exposed in the base of all satisfactory foundation excavations should be protected against any detrimental change in conditions such as disturbance from rain, frost or groundwater seepage. Surface runoff should be diverted away from the footing trench excavations and not be allowed to pond. Water encountered within the footing trench excavation should be pumped out prior to backfilling or concrete placement.

7.6 Seismic Considerations

The project location is determined to be Site Class D as per AASHTO (2012), Section 3.10.3.1. The maximum considered earthquake spectral response acceleration at short period, S_s (0.2 seconds) is 0.320 g and S1 (1.0 second) is 0.092 g. The values of site factor coefficients F_a , and F_v for Site Class D is approximately 1.54 and 2.41 respectively. Peak ground acceleration, PGA, for this site is 0.186.

7.7 Lateral Earth Pressures

Earth pressures will be influenced by the structural design of the walls, methods of construction and compaction, the strength of the materials being restrained, and the conditions of wall restraint. The lateral earth pressure design parameters for retaining wall work should be designed to withstand lateral earth pressures caused by adjacent soil and surcharge load. If low plasticity cohesive soil is used as backfill, the earth pressure against the walls may be computed using the following equation:

 $P_{\rm h} = 45 {\rm H} + 0.6 {\rm Q}$

Where: $P_h =$ lateral earth pressure at any depth h, psf

H = depth below adjacent grade, feet

Q = surcharge loads, psf

8 GLOBAL STABILITY OF RETAINING WALL SLOPE

For global stability of a slope, the following information should be considered: Geometry (cross section and loading conditions); Location of the water table; soil / rock stratigraphy; soil/rock properties (unit weight, Atterberg Limits, undrained and drained shear strength); Additional

loading conditions (traffic surcharge, railroad live load, etc.). For the soils in this location (classified as CL) a reference value of 300 psf for cohesion and a phi angle of 20 degrees are acceptable for global stability analysis. If using the NAVFAC DM-7.2 (1982) graphical reference, use curve 3 for the active components for retaining walls (k_v and k_h).

For global stability of a slope, a minimum factor of safety $FS \ge 1.3$ is recommended for both the long-term drained condition and the short term undrained condition, except recommend making the factor of safety 1.5 for slope or walls that support buildings, critical utilities, or other installations with a low tolerance for failure.

With a minimum soil reinforcement length behind the *MSE* retaining wall of 1.0 x Height of *wall*, slope stability analysis *for the preliminary wall plans (see Appendix D)* yielded a factor of safety of 2.146 for non-earthquake loaded condition and 1.477 for earthquake loaded condition (see Appendix C) and for the updated wall plans (see Appendix D) yielded a factor of safety of 3.236 for non-earthquake loaded condition and 1.995 for earthquake loaded condition (see Appendix C).

9 ROAD CONDITION ASSESSMENT

On September 14, 2020, ABNA obtained 3 pavement cores roughly at the third points within the project. Cores were extended through the aggregate base and into the sub base. The following are observations of the core samples:

		PAVEMENT	AGGREGATE	TOTAL	BEARING
CORE	LOCATION	THCIKNESS	THICKNESS	DEPTH	STRENGTH
1	CL 17+60	8.5 inches	6.5 inches	17 inches	25,800 psf
2	PCC 302+50	8.5 inches	4.0 inches	13 inches *	24,800 psf
3	PCC 200+30	8.5 inches	5.5 inches	21 inches	29,800 psf

* hand auger encountered rock and resulted in auger refusal.

10 GENERAL REMARKS/REPORT LIMITATIONS

This report has been prepared for the exclusive use of **Horner & Shifrin, Inc.**, for the specific application to the subject project. All recommendations contained in this report have been made in accordance with generally accepted soil and foundation engineering practices. No other warranties are implied or expressed.

The analysis and recommendations submitted in this report are based in part upon the data obtained from the test borings. The nature and extent of variations between the borings may not become evident until construction. If variations appear to be evident, it may be necessary to re-evaluate the recommendations of this report.

We emphasize that this report is for design purposes only and may not be sufficient to prepare an accurate bid. Contractors reviewing this report should acknowledge that the discussions and recommendations contained herein are for design purposes.

When the plans and specifications are more complete, or if significant changes are made in the nature of the proposed project, a consultation should be arranged to review them with respect to prevailing soil conditions. At that time, it may be necessary to submit supplementary recommendations.

We also suggest that the geotechnical engineer be granted the opportunity to review the plans and specifications to verify that the recommendations in this report are properly interpreted and incorporated in the design. If the geotechnical engineer is not granted the privilege of making this recommended review, the geotechnical engineer can assume no responsibility for misinterpretation of his recommendations.

FIGURES



Figure 1: Google Maps image of Little Hills Expressway – Plan View

Site Overview and Borehole Locations



Figure 2: Web Soil Survey image of site.

Site Overview and Borehole Location

APPENDIX A

APPENDIX A1 - SUMMARY OF LABORATORY TESTING

Laboratory testing was performed on selected representative samples to evaluate pertinent engineering properties of the soils. To supplement the visual classification of the soil samples, the following tests were performed. These laboratory tests were performed in accordance with applicable ASTM standards.

A1.1 Natural Moisture Contents

Natural moisture contents were evaluated on selected samples. The natural moisture content is the ratio, expressed as a percentage, of the weight of water in a given amount of soil to the weight of soil particles. The results are indicated on the Logs of Boring and Summary of Laboratory Results in Appendix B.

A1.2 Atterberg Limits

Atterberg limits tests were performed to evaluate the soil's plasticity characteristics. The soil's Plasticity Index (P.I.) is representative of this characteristic and is bracketed by the Liquid Limit (L.L.) and the Plastic Limit (P.L.). The Liquid Limit is the moisture content at which the soil will flow as a heavy viscous fluid. The Plastic Limit is the moisture content at which the soil is between the "plastic" and the semi-soil stage. The results of these tests are presented on Logs of Boring and Summary of Laboratory Results in Appendix B. The Plasticity Index (P.I. = L.L. - P.L.) is a frequently used indicator for the soil's potential for volume change. Typically, volume change potential increases with higher plasticity indices.

A1.3 Pocket Penetrometer

Pocket Penetrometer (P.P.) tests were performed on cohesive soil samples. The Pocket Penetrometer provides a consistency classification and an indication of the soil's unconfined compressive strength. Due to the sampling method described below, the upper sample was tested in the boring wall. The lower sample was tested on the largest pieces available and averaged. This method results in values that can only be classified as an estimate.

APPENDIX A2 - DRILLING AND SAMPLING PROCEDURES

Soil drilling and sampling operations were conducted in general accordance with ASTM D1586-11. The borings were advanced by mechanically twisting continuous hollow stem auger flights into the ground. Samples were obtained with a standard 2 inch O.D. split-barrel sampler. The sampler was driven a typical total of 18 inches by means of a 140 pound C.M.E. auto-hammer with a free fall of 30 inches. The number of hammer blows required to drive the sampler the final 12 inches of penetration was recorded and designated as the standard Penetration Test "N-Value". The penetration resistance, when properly evaluated, is an index to the in-situ relative density of cohesionless soils, the consistency of cohesive soils, the behavior under applied loads, and the relative hardness of bedrock.

Rock drilling and sampling operations were conducted in general accordance with ASTM D2113-14. Drilling is accomplished by circulating a drilling medium through the drill bit while rotating and lowering or advancing the string of drill rods as downward force is applied to a cutting bit. The bit cuts and breaks up the material as it penetrates the formation, and the drilling medium picks up the cuttings generated by the cutting action of the bit. The drilling medium, with cuttings, then flows outward through the annular space between the drill rods and drill hole, and carries the cuttings to the ground surface, thus cleaning the hole. The string of drill rods and bit is advanced downward, deepening the hole as the operation proceeds. Coring is the process of recovering cylindrical cores of rock by means of rotating a hollow steel tube (core barrel) equipped with a coring bit. The drilled core is carefully collected in the core barrel as the drilling progresses. Once the core has been cut and the core barrel is full, the drill rods or overshot assembly are pulled and the core retrieved. The core samples recovered were measured in the field for percent recovery and Rock Quality Designation value (RQD). Each core sample was placed in a cardboard box for transport to the laboratory. The sampling sequence for each coring is summarized on the appropriate Log of Boring in Appendix C1 as well as shown on an annotated core log in Appendix C2. The boreholes were completed with cuttings or grout at depth and grouted or chipped near the surface with spider plugs supporting asphalt patches when needed until the grout fully cured.

APPENDIX B

APPENDIX B1

Log of Borings

9	- ^		1.4											SHEET 1	OF 1
I	A	RL	N A	1		٦	AILY	FIELD	REPOR	RT BOF	REHOLE LOC	3		PROJECT	NUMBER: 19-6023
														HOLE NUN	IBER: B-1
PROJE	CT: Little	Hills E	xpress	way						LOCA	TION:				
COORE	DINATES:									DRILL	ING CONTR	ACTOR: Bull	dog Drilling		1
	MAKE AN	ID MOE	DEL: C	ME 5	55LC	DEPT	'H TOF	P OF R	OCK:	N/A		DEPTH CA	SING & SIZE:	3¾"	HOLE SIZE: 7"
ELEVA	TION: 54	3.36			ANGLE FROM VER	T. AND	BEAR	RING:	N/A			DEPTH BO	TTOM OF HC	DLE: 20'	1
WATER	LEVEL:	N/A			FLUIDS AND ADDIT	TIVES:	N/A				DATE STAR	RT: 8/17/20	DATE FINIS	iH: 8/17/20	LOGGER: AJS
	NO.	S.	AMPL	E	STANDARD	0				ы			SOIL DESC	RIPTION	
NOI	BEL (Ř	×	PENETRATION TEST RESULT	CLO	3E %	TIMI	LIMIT	QNI					
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EL	G Feet	INTE	TYPE & N	RECO	Pocket Penetrometer tons/ft²	cket S S S S S S S S S S S S S S S S S S S								CTURE, MIN YMBOL	ERALOGY, USCS
	0				1										
	1														
	2	1-2.5	SS-1	18"	1-1-2	-	28.20				Soft, Brown	Clayey Silt			
	3	-													
	4	3.5-5	SS-2	14"	1-2-2		28.56				Soft, Brown C	Clayey Silt (ML	-)		
	5	-			1.50	1									
	6	-													
	1														
	8														
	9	8.5-10	SS3	18"	1-2-2	-	31.13				Soft Grav Sil	tv Clav			
	10				0.23						oon, ondy on	iy olay			
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	13	-													
	14	12 5 15	664	19"	012		30.18								
	45	10.0-10	0.04	10	0.50	1	00.10				Soft, Gray Sil	ty Clay			
	15														
	16														
	17	1													
	18														
	19	18.5-20	SS5	18"	1-1-3 0.75		27.29				Soft, Gray Cla	ayet Silt	Boring termin	ated at 20'	
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1															

2														SHEET	1 OF 3
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														HOLE NUN	IBER: B-2
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COORD	INATES:									DRILL	ING CONTR	ACTOR: Bul	ldog Drilling	9 Millio (1940-1945)	1
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ELEVAT	10N: 554	4.58'			ANGLE FROM VER	T. ANE	BEAF	RING:	N/A			DEPTH BC		DLE: 60'	
WATER	LEVEL:	N/A			FLUIDS AND ADDIT	IVES:	N/A				DATE STAR	RT: 8/14/20	DATE FINIS	SH: 8/14/20	LOGGER: AJS
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	14	13.5-15	SS3	18"	4-4-4		27.79				Medium Stiff,	Orange Brow	n Silty Clay	2" hand of	Clavov Silt
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	19	18.5-20	SS4	18"	1-2-3 0.50	-	34.87				Soft, Clayey S	Silt, transition	from Brown to	Gray	
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WATER	LEVEL:	N/A			FLUIDS AND ADDIT	TIVES:	N/A				DATE STAR	RT: 8/14/20	DATE FINIS	H: 8/14/20	LOGGER: AJS
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	25														
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	29	28.5-30	SS6	18"	0-1-2		27.94				Soft, Gray Sil	ty Clay			
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	32														
	33														
	34	33.5-35	SS7	18"	1-3-3	-	26.48				Medium Stiff,	Gray Silty Cla	ay		
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		1D MOE	EL: C	CME 5	55LC	DEPT	'H TOF	OF R	OCK:	N/A		DEPTH CA	SING & SIZE:	3¼ HAS	HOLE SIZE: 7"
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	49	48.5-50	SS10	18"	2-4-4	-	25.98				Very Stiff, Bro	wn with Gray	Clay		
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	51	1													
	52	-													
	53	-													
	54	53.5-55	SS11	18"	2-4-4		26.50				Very Stiff, Bro	own Clay			
	55				2.25	1	20.00								
	55														
	56														
	57	1													
	58	1													
	59	58.5-60	SS12	18"	3-5-7 3.50	-	23.12				Very Stiff, Mo	ttled light and	l dark Brown Sil	lty Clay Boring Term	inated at 60'
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WATER	LEVEL:	N/A			FLUIDS AND ADDI	TIVES:	N/A				DATE STAR	T: 8/17/20	DATE FINIS	H: 8/17/20	LOGGER: AJS
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	0														
	4	35-5	SS-1	16"	2-2-3		25.82				Soft, Brown S	ilty Clay			
	5				1.25	1									
	6														
	7														
	8	1													
	9	8.5-10	SS2	15"	7-7-9	4	10.49				Dry, Brown Lo	Dess			
	10	1			MAX										
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	14						10.05								
	14	13.5-15	553	16"	3.75	1	10.38				Dry, Brown L	1692			
	15														
	16]													
	17	1													
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	19	18.5-20	SS4	16"	3-3-5	-	17.04				Dry, Brown Lo	Dess			
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9	5					L		IELD	REPU			2		PROJECT	NUMBER: 19-6023
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ATION	TH BELOV	VAL	MBER	ERY	STANDARD PENETRATION TEST RESULT	DLIC LOG	TURE %	ID LIMIT	IIC LIMIT	XITY INDEX	NAI	ME, GRADA	TION OR PLA	STICITY, PA	RTICLE SIZE
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	31	1													
	32	1													
	33	1													
	34	33.5-35	SS7	18"	1-2-3	-	26.14	33	21	12	Soft, Gray Sill	ty Clay (CL)			
	35	1			1.75										
	36														
	37														
	38														
	39	38.5-40	SS8	18"	2-3-4		25.99				Medium Stiff,	Gray Silty Cla	ay		
REMAR	KS:				3.0										
The stratifica In situations	itions lines re the transition	present app may be gra	oroximate adual.	e strata b	xoundaries .										

1	<u>(</u> A)	BN	14	A		C	AILY	FIELD	REPOR	RT BOF		9		SHEET 3 PROJECT I	OF 3
)														HOLE NUM	BER: B-3
PROJE	CT: Little	Hills Ex	xpress	sway						LOCA	TION:				
COORE	INATES:									DRILL	ING CONTR/	ACTOR: Bull	dog Drilling		-
	/AKE AN	D MOD	EL: C	CME 5	55LC	DEPT	'H TOF	POFR	OCK: I	N/A		DEPTH CA	SING & SIZE:	31/4 HAS	HOLE SIZE: 7"
ELEVA	FION: 556	5.27'			ANGLE FROM VER	T. ANE	BEAF	RING:	N/A			DEPTH BO	TTOM OF HO	LE: 45'	
WATER	LEVEL:	N/A			FLUIDS AND ADDIT	TIVES:	N/A				DATE STAR	RT: 8/17/20	DATE FINIS	H: 8/17/20	LOGGER: AJS
	M	SA	AMPL	E	STANDARD					X			SOIL DESC	RIPTION	
VATION	PTH BELC SURFACE	RVAL	JMBER	VERY	PENETRATION TEST RESULT	OFIC FOG	STURE %	JID LIMIT	TIC LIMIT	CITY INDE	NAI DISTRIBUT	ME, GRADA TON, COLOI	TION OR PLA R. MOISTURE	STICITY, PA	RTICLE SIZE RELATIVE DENSITY
ELE	Feet	INTEF	YPE & NL	RECO	Pocket Penetrometer tons/ft²	SYMB	MOIS	רומר	PLAS	PLASTI	OR COI	VSISTENCY	, SOIL STRUC GROUP S	CTURE, MIN YMBOL	ERALOGY, USCS
	41														
	43														
	44	43.5-45	SS9	18"	3-3-5	-	25.66				Medium Stiff,	Dark Gray Si	lty Clay Boring termin	ated at 45'	
	45														
	46														
	47														
	48														
	49														
	50														
	50														
	51														
	52	1													
	53														
	54														
	55														
	56														
	57														
	50														
	56														
	59														
REMAR The stratifica In situations	KS: ations lines re the transition	present app may be gra	eroximate Idual.	strata b	ooundaries .										

1	SAI	BN	1A	4		D	AILYF	IELD	REPOR	rt Bof	REHOLE LOO	3		SHEET 1 PROJECT N	OF 3 NUMBER: 19-6023
											TION			HOLE NUM	BER: B-4
PROJEC		HIIIS E	xpress	sway						LOCA			_		
COORD	INATES:	:									ING CONTR/	ACTOR: Bui	dog Drilling		
	/IAKE AN	ID MOE	DEL: C	CME 5	55LC	DEPT	'H TOP	OF R	OCK: I	N/A		DEPTH CA	SING & SIZE:	3% HAS	HOLE SIZE: 7"
ELEVAT	FION: 556	5.89'			ANGLE FROM VER	T. ANE	BEAR	RING:	N/A			DEPTH BO	TTOM OF HO	DLE: 45'	1
WATER	LEVEL:	N/A			FLUIDS AND ADDIT	TIVES:	N/A				DATE STAR	RT: 8/17/20	DATE FINIS	SH: 8/17/20	LOGGER: AJS
VIION	H BELOW RFACE	S AL		RY m	STANDARD PENETRATION TEST RESULT	IC LOG	URE %) LIMIT	C LIMIT	TY INDEX	NAI	ME, GRADA	SOIL DESC	STICITY, PA	RTICLE SIZE
TEV/	SU	ERV	MUN	OVE		MBOL	DISTI	auic	ASTIC	LICI.	DISTRIBUT OR COI	TON, COLOI VSISTENCY	R, MOISTURE	E CONTENT, CTURE, MIN	RELATIVE DENSITY ERALOGY, USCS
	Feet	- II	TYPE &	REC	Pocket Penetrometer tons/ft ²	SYI	Ň		4	PLAS			GROUP S	YMBOL	
REMAR	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 KS: Borin	3.5-5 8.5-10 13.5-15	SS-1	15" 16" 17"	4-5-5 0.5 5-3-6 1.25 4-3-4 1.75 2-3-3 1.50 rately 1' lower than or	- - - iginal 6	27.74 23.94 23.62 25.43 Ievatio	36 n due	22 to level	14	Brown Loess Brown Loess Brown Loess Gray Silty Cla	ay (CL) g placement			
REMAR The stratifica In situations	KS: Borin tions lines re the transition	ng start present app may be gra	ed app proximate adual.	strata b	1.50 nately 1' lower than or oundaries .	 iginal e	elevatio	n due	to level	ing of ti	e slope for ri	g placement			

8	< ^ \		1.4											SHEET 2	OF 3
E		BN	1 F	1		D	AILYF	IELD	REPO	rt Bof	REHOLE LOO	3		PROJECT	NUMBER: 19-6023
											TION			HOLE NUM	BER: B-4
PROJEC	CT: Little	e Hills E	xpress	sway						LOCA					
COORL									0.01/		ING CONTRA			01/110.0	
			EL: (N/A		DEPTHCA	SING & SIZE:	3% HAS	HOLE SIZE: 7"
ELEVA	1011:55	6.89			ANGLE FROM VER		BEAR	(ING:	N/A		DATE OTAE			LE: 45	
WATER	LEVEL:	N/A		_	FLUIDS AND ADDI		N/A			1	DATESTAR	(1:8/17/20		H: 8/17/20	LUGGER: AJS
ATION	TH BELOW URFACE	/AL	ABER	ERY	STANDARD PENETRATION TEST RESULT	DLIC LOG	rure %	D LIMIT	IC LIMIT	ITY INDEX	NAI	ME, GRADA	TION OR PLA	STICITY, PA	RTICLE SIZE
ELEV	G G Feet	INTER	rPE & NUN	RECOV	Pocket Penetrometer tons/ft ²	SYMBO	NOIS	ΓΙΔΠΙ	PLAST	PLASTIC	OR COI	VSISTENCY	, MOISTURE SOIL STRUC GROUP S	YMBOL	RELATIVE DENSITY ERALOGY, USCS
<u> </u>	20		F												
	21														
	25	20.0-20	555	10	1.5	1	20.40				incularit etili,	only only on	-)		
	25														
	26														
	27														
	28														
	29	28.5-30	SS6	18"	4-4-5		26.73				Stiff Gray Silt	y Clay			
	30				2.0										
	31														
	32	-													
	33														
	34	33 5 35	557	18"	1-2-3		28.45				Medium Stiff	Grav Silty Cla	av		
	35	00.0-00	507	10	0.5	1	20.40								
	30														
	36														
	37														
	38														
	39	38.5-40	SS8	18"	1-2-3	-	28.47				Medium Stiff,	Stiff Brown S	ilty Clay		
REMAR	KS:	1			1.25										
The stratifica In situations	ations lines re the transition	present app may be gra	roximate idual.	strata b	oundaries .										

0														SHEET 3	OF 3
1	A	SL	1 A	4		D	AILY	IELD	REPOR	RT BOF	REHOLE LOG	3		PROJECT	NUMBER: 19-6023
)														HOLE NUM	BER: B-4
PROJEC	CT: Little	Hills Ex	xpress	sway						LOCA	TION:				
COORD	INATES:									DRILL	ING CONTRA	ACTOR: Bulk	dog Drilling		
DRILL N	1AKE AN		EL: C	CME 5	55LC	DEPT	'H TOF	OF R	OCK: I	A/V		DEPTH CAS	SING & SIZE:	3% HAS	HOLE SIZE: 7"
ELEVAT	'ION: 556	6.89'			ANGLE FROM VER	T. ANE	BEAF	RING:	N/A			DEPTH BOT	ITOM OF HC	DLE: 45'	
WATER	LEVEL:	N/A			FLUIDS AND ADDIT	IVES:	N/A				DATE STAR	T: 8/17/20	DATE FINIS	H: 8/17/20	LOGGER: AJS
	M	S/	AMPL	E	STANDARD					X			SOIL DESC	RIPTION	
Z	BELO ACE		ъ		PENETRATION	00	Ж Ш	MIT	TIMI	INDE					
VATI	SURF	RVAL	IMBE	VERY	IEST RESULT	OLIC	STUR	I DI	TICL	CITY	NAI DISTRIBUT	NE, GRADAT ION, COLOR	TON OR PLA	STICITY, PA	RTICLE SIZE RELATIVE DENSITY
ELE	8	NTEF	& NL	ECO.	Pocket	× WB	MOIS	ПаГ	PLAS	ASTI	OR COM	VSISTENCY,	SOIL STRUG	TURE, MINI	ERALOGY, USCS
	Feet Feet														
	40														
41															
42															
43															
	44	43.5-45	559	18"	2-2-3		25.39				wedium Sun,	Orange Brown	Boring termin	ated at 45'	
	45														
	46	1													
	47														
	48														
	49														
	50														
	50														
	51														
	52														
	53														
	54														
	55														
	56														
	57														
	50														
	50														
	59														
REMAR The stratifica In situations	KS: tions lines rep the transition	present app may be gra	roximate idual.	strata b	, oundaries .										

0															05 3
	(A)	BN	JA	4		C		FIELD	REPO	RT BOF	REHOLE LOO	3		SHEET T	
4	5													PROJECT	NUMBER: 19-6023
PROJE	CT: Little	Hills E	xpress	swav						LOCA	TION:			HOLE NUM	BER: B-5
COORE	INATES:		1							DRILL	ING CONTR	ACTOR: Bul	ldoa Drillina		
			DEL: C	CME f	55I C	DEPT		OFR	OCK:	41'		DEPTH CA	SING & SIZE:	3% HAS	HOLE SIZE: 7"
FLEVA		3 22'					BEAR		N/A			DEPTH BC		DLE: 45'	
WATER		N/A					N/A					T· 8/17/20		H: 8/17/20	LOGGER: AIS
		s		E									SOIL DESC	RIPTION	
ATION	TH BELOW	VAL	MBER	ERY	STANDARD PENETRATION TEST RESULT	DLIC LOG	TURE %	D LIMIT		XITY INDEX	NAI	ME, GRADA	TION OR PLA	STICITY, PA	RTICLE SIZE
ELEV	Feet	INTER	YPE & NUI	RECOV	Pocket Penetrometer tons/ft ²	SYMBO	NOIS	ΓΙΔΝ	PLAST	PLASTIC	OR COI	VSISTENCY	, SOIL STRUG GROUP S	YMBOL	ERALOGY, USCS
	1														
	2														
												Piltu Clou with	limostopo grou		
	-	3.5-5	55-1	9	4-3-4 N/A	1	18.02				FILL, BIOWIN	Silly Cidy With	ninestone grav	er	
	5														
	6														
	7	1													
	8														
	9	8.5-10	SS2	16"	3-3-3		34.39				Stiff, Dark Gr	ay Silty Clay			
	10				1.50										
	11	-													
	12														
	12														
	15														
	14	13.5-15	SS3	18"	2-2-1 0.75	{	33.59				Soft, Brown a	ind Gray Clay	ey Silt		
	15	1													
	16														
	17														
	18														
	19	18.5-20	SS4	18"	0-1-1		50.00				Very Soft, Gr	ay Silty Clay			
REMAR The stratifica In situations	KS: Borin ations lines rep the transition	ng start present app may be gra	ed app proximate adual.	oroxin strata b	nately 1' lower than or	riginal e	levatio	n due	to level	ling of t	he slope for ri	g placement	i.		

9														SHEET 2	OF 3
T	A	RV	1 A	1		۵	AILY F	IELD	REPOR	rt Bof	REHOLE LOG	3		PROJECT	UMBER: 19-6023
)														HOLE NUM	BER: B-5
PROJEC	CT: Little	e Hills E	xpress	sway						LOCA	TION:				
COORD	INATES	:								DRILL	ING CONTRA	ACTOR: Bull	dog Drilling		
	IAKE AN		EL: C	CME 5	i5LC	DEPT	'H TOP	OFR	OCK:	41'		DEPTH CAS	SING & SIZE:	3% HAS	HOLE SIZE: 7"
ELEVAT	10N: 45	8.22'			ANGLE FROM VER	T. ANE	BEAR	ING:	N/A			DEPTH BO	FTOM OF HC	DLE: 45'	
WATER	LEVEL:	N/A			FLUIDS AND ADDIT	IVES:	N/A				DATE STAR	RT: 8/17/20	DATE FINIS	H: 8/17/20	LOGGER: AJS
	×	S	AMPL	E						×			SOIL DESC	RIPTION	
/ATION	TH BELO	VAL	MBER	ERY	PENETRATION TEST RESULT		TURE %	ID LIMIT	TIC LIMIT	SITY INDE	NAI	ME, GRADAT	TION OR PLA	STICITY, PA	RTICLE SIZE
										ASTIC	OR COI	VSISTENCY,	SOIL STRU	CTURE, MINI	ERALOGY, USCS
$\begin{array}{c c c c c c c c c c c c c c c c c c c $										PL			GROUP 3	INBOL	
	20		-												
	21	-													
	22	-													
	23														
	24	23.5-25	SS5	18"	0-1-1 0.50		71.79				Soft, Gray Sil	ty Clay with Bl	ack Organics		
	25														
	26														
	27														
	28	-													
	29	28.5-30	SS6	18"	0-0-0		61.55				Very Soft, Gra	ay Silty Clay			
	30	-			0.25	1									
	24														
	31														
	32														
	33										Verv Soft. Gra	av Siltv Clav			
	34	33.5-35	SS7	18"	0-0-1		48.56				Soft Cray Sil	ty Clay with S	and starting at	24.5	
	35	1			0.25						Son Gray SI	ty Clay with Sa	ing starting at	Rottery Drillin	g from 35'
	36	-													
	37	-													
	20	4													
	- 30														
	39	38.5-40	SS8	13"	4-16-15						Fine to Mediu	m Grained Sa	nd and Limest	one gravel	
REMAR The stratifica In situations	KS: tions lines re the transition	epresent app n may be gra	oroximate Idual.	strata b	, oundaries.										

															OF 3			
ABNA							DAILY FIELD REPORT BOREHOLE LO							PROJECT NUMBER: 19-6023				
<u> </u>													HOLE NUMBER: B-5					
PROJEC	CT: Little	Hills E	xpres	sway				LOCATION:										
COORD	COORDINATES:																	
DRILL N	DRILL MAKE AND MODEL: CME 55LC DEPTH TOP OF ROCK: N										A DEPTH CASING & SIZE: 3% HAS HOLE SIZE: 7"							
ELEVATION: 458.22' ANGLE FROM VERT. AND BEARIN									N/A			DEPTH BO	TTOM OF HO	LE: 45'				
WATER		FLUIDS AND ADDI	TIVES:	N/A				DATE START: 8/17/20 DATE FINISH: 8/17/20 LOGGER: AJS										
	M	SAMPLE								×			SOIL DESC	RIPTION				
ELEVATION	DEPTH BELO SURFACE	INTERVAL	YPE & NUMBER	RECOVERY		SYMBOLIC LOG	MOISTURE %	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDE	NAME, GRADATION OR PLASTICITY, PARTICLE SIZE DISTRIBUTION, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY, USCS GROUP SYMBOL							
	40									Green Shale fragments in drilling return								
	42 43 44 45	41.5' to 46.5'	Run 1 60/6		RQD 45/60 75% Fair to Good						Top of core barrel Contained Coarse Grained, Rounded Gravel Limestone: Moderately Hard, Finely Crystaline, Thick Bedded, Sligthly Weathered, Dense, Good Quality Gray Shale: 44' to 44.2'							
	46	 				-							Boring termin	ated at 46.5				
	47										-	<u>113 5 10 7 8</u>	9.110.11	2 3 4 5	CP 7 B R 10 H			
	48										-				ALL			
	49											Concession of the		1	Management Ma			
	50												- Aller	ahass of	ALL CALL			
	50										(pt)	A COLORAD IN	B-5 Run 1: 41.5	' to 46.5'				
	51																	
	52																	
	53	1																
	54																	
	55	-																
	56	-																
	57	-																
	58																	
	59																	
REMAR The stratifica In situations	KS: ations lines re the transition	present ap may be gr	proximate adual.	e strata b	cundaries .													

9													SHEET 1	OF 1				
1	A	1		D	AILYF	IELD	REPOR	RT BOF	REHOLE LOG	3		PROJECT NUMBER: 19-6023						
<u> </u>													HOLE NUMBER: B-6					
PROJECT: Little Hills Expressway											LOCATION:							
COORD	COORDINATES:											DRILLING CONTRACTOR: Bulldog Drilling						
	DRILL MAKE AND MODEL: CME 55LC DEPTH TOP OF ROCK: N											N/A DEPTH CASING & SIZE: 3% HAS HOLE SIZE: 7"						
ELEVATION: 518.60' ANGLE FROM VERT. AND BEARING: N/A											DEPTH BOTTOM OF HOLE: 10'							
WATER LEVEL: N/A FLUIDS AND ADDITIVES: N/A											DATE STAR	ATE START: 8/14/20 DATE FINISH: 8/14/20 LOGGER: AJS						
	N	SAMPLE								×			SOIL DESC	RIPTION				
'ATION	DEPTH BELO DEPTH BELO	VAL	MBER	ERY	PENETRATION TEST RESULT	SYMBOLIC LOG	MOISTURE %	ID LIMIT	TIC LIMIT	PLASTICITY INDE	NAME, GRADATION OR PLASTICITY, PARTICLE SIZE DISTRIBUTION, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY, USCS GROUP SYMBOL							
ELE		INTER	YPE & NU	RECO	Pocket Penetrometer tons/ft ²			ПаU	PLAS									
	0		-								Grass, approx	kimately 1' Top	o Soil					
	1	1-2.5	SS-1	12"	2-2-3	-	23.98				Medium Stiff, Brown Silty Clay							
	2				1.25													
	3	3																
	4 3.5-5 SS-2 16" <u>3-3-4</u> 20.52						Imedium Stiff, Brown Silty Clay											
	5]																
	65-8 SS3 18" 2-3-4 29.48						Medium Stiff, Brown Silty Ck											
	7 1.5																	
	9	8.5-10	SS4	18"	2-3-4		23.14				Medium Stiff,	Brown Silty C	ay					
	10				2.25								Boring termin	ated at 10'				
	11	-																
	12																	
	12	-																
	14	-																
	15																	
	15																	
	16																	
	17																	
	18]																
	19																	
REMAR The stratifica In situations	REMARKS: The stratifications lines represent approximate strata boundaries . In strations the transition may be gradual.																	

9					SHEET 1 OF									OF 1				
									REPOR	rt Bof	REHOLE LOG	3	PROJECT NUMBER: 19-6023					
)													HOLE NUMBER: B-7					
PROJEC	CT: Little	Hills E	xpress	sway				LOCATION:										
COORD	INATES							DRILLING CONTRACTOR: Bulldog Drilling										
	DRILL MAKE AND MODEL: CME 55LC DEPTH TOP OF ROCK: N											DEPTH CASING & SIZE: 3% HAS HOLE SIZE: 7"						
ELEVAT	ELEVATION: 546.69' ANGLE FROM VERT. AND BEARING: N/A											DEPTH BOTTOM OF HOLE: 15'						
WATER	WATER LEVEL: N/A FLUIDS AND ADDITIVES: N/A										DATE STAR	T: 8/14/20	DATE FINIS	H: 8/14/20	LOGGER: AJS			
	3	S	AMPL	E	STANDARD PENETRATION TEST RESULT	DLIC LOG	MOISTURE %			PLASTICITY INDEX			SOIL DESC	RIPTION				
ATION	TH BELO	/AL	MBER	ERY				D LIMIT			NAME, GRADATION OR PLASTICITY, PARTICLE SIZE DISTRIBUTION, COLOR, MOISTURE CONTENT, RELATIVE DENSITY OR CONSISTENCY, SOIL STRUCTURE, MINERALOGY, USCS GROUP SYMBOL							
ELEV	DEF	LTER	YPE & NUN	ECOV	Pocket	YMBO		ΠαυΙ	PLAS									
	Feet	_ ≤		8	Penetrometer tons/ft ²	co												
	0								6 " Asphalt 4	" aggregate ba	se							
	1	-					29.83											
	2	1-2.5	SS-1	16"	0-2-1						Soft, Brown Silty Clay							
	3																	
	4	3.5-5	SS-2	18"	2-2-3 0.75		28.82				Medium Stiff,	Brown Silty Cl						
	5]																
	6									Medium Stiff, Brown Clevey								
	7	0.0-0	555	10	0.50		22.02				Medium oun,	blown oleyey						
	8																	
	9	8.5-10	SS4	18"	1-2-3		30.61				Medium Stiff,	Brown Silty Cl	ay					
	10	-			0.50	1												
	11	-																
	10																	
	12																	
	13																	
	14	13.5-15	SS5	186	3-2-2		30.04				Medium Stiff,	Brown Clayey	Silt Boring Termin	nated at 15'				
	15																	
16 17																		
	19	-																
	KS. Ber		mour	dana	rovimately 75' South	orto	the cho	uldor	due to	conflict	with utilities							
The stratifica	tions lines re the transition	present app may be gra	proximate adual.	strata b	oundaries.	, 911.01		ulder,		oon not	, min dundes							

APPENDIX C

APPENDIX C1

Slope Stability Analysis



Slope Stability Analysis of Preliminary Plan Profiles (Appendix D1).



Slope Stability Analysis with earthquake loading *of Preliminary Plan Profiles* (*Appendix D1*).



Slope Stability Analysis of Updated Plan Profiles (Appendix D1).



Slope Stability Analysis with earthquake loading of Updated Plan Profiles (Appendix D1).

APPENDIX D

APPENDIX D1

Wall Sheet Plan Profiles

ABNA Engineering Inc. 4140 Lindell Blvd, St. Louis MO

Geotechnical Report rev 1 Little Hills Expressway, St. Charles



Preliminary Plan Wall Sheet - 2/21/2020

ABNA Engineering Inc. 4140 Lindell Blvd, St. Louis MO

Geotechnical Report rev 1 Little Hills Expressway, St. Charles



Updated Plan Wall Sheet - 10/21/2021